SLUDGE BUILD-UP IN SEPTIC TANKS, BIOLOGICAL DIGESTERS AND PIT LATRINES IN SOUTH AFRICA

Report to the Water Research Commission

by

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EXECUTIVE SUMMARY

The objective of this project was to establish sludge build up rates in various on-site sanitation systems under South African conditions. The sludge build up rate is an important design criterion in sizing on-site sanitation systems, for example septic tanks, pit latrines, etc. Comparison of data obtained on various other projects carried out by CSIR Building and Construction Technology (Boutek), indicated that the design criteria currently in use in South Africa were generally inappropriate because they are based largely on experience in other countries. There are many factors affecting the performance of on-site sanitation systems which have not been sufficiently quantified. Climatic and socio-economic factors, for instance, play a major role in the rate of sludge build up, and these differ from country to country. It is not satisfactory, therefore, to simply apply design criteria applicable to other countries. Furthermore, claims by commercial manufacturers of on-site sanitation systems about the design life of their products needed appraisal.

The project commenced with a literature survey which yielded mainly information concerning septic tanks. Less data on pit latrines was available. Factors considered to affect the rate of sludge build up were generally considered to be the number of users, anal cleansing materials used, diet, soil conditions, seasonal effects (temperature, moisture, etc), retention time, influent characteristics and toilet cleaning materials.

Boutek designed a perspex sampling tube which enabled a core to be taken of septic tank and digester contents, from which the depth of sludge could be directly measured and the clarity of the liquid layer established. The contents of VIP latrines were measured by lowering a steel tape with a weight into the pit and measuring the average depth from the toilet seat to the sludge.

The project measured the sludge build up rate in VIP latrines at Constantia Park and Soshanguve (Pretoria), septic tanks at Marselle (Eastern Cape) and Warden (Free State) as well as two kinds of "Loflo" digesters at Umbumbulu (Durban) and Ivory Park (Midrand). Various problems which affected the capture of data were experienced during the monitoring programme; these mostly concerned aspects such as tank emptying routines, reliable information on the number of users, the improper emptying of tanks, as well as political instability. Despite these problems, however, sufficient information was obtained for the purpose of establishing acceptable design guidelines.

The research enabled the following predictions for average sludge build up rates to be recommended:

VIP latrines:

0.07 litres/person/day

• Septic tanks and "Loflo" systems:

0.08 litres/person/day

It was furthermore possible to suggest that provision for scum accumulation is not necessary. Outlet T-pieces are, however, essential items of equipment.

The research also yielded some important aspects on which recommendations could be made:

- User education is of crucial importance in order to ensure correct operation and maintenance of sanitation systems;
- correct installation of sanitation systems should be enforced by quality control on site;
- tanks connected to Loflo systems should have a minimum volume of 1 000 litres, while tanks receiving sullage in addition to toilet wastes should be at least 1 750 litres; and
- pits for VIP toilets should be as large as possible in order to reduce desludging frequencies, given site and cost constraints.

It is also recommended that further research be conducted into the optimum size for Loflo sanitation systems, as it is suspected that 1 000 litres may be inadequate. Additionally, there is an urgent need for research and information dissemination on low-maintenance sanitation systems, as many local authorities have insufficient funds to carry out maintenance tasks properly.

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PROJECT TEAM

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LIST OF SYMBOLS

| l | litre |
|-----|---|
| p | person |
| d | day |
| yr | year |
| k | permeability |
| n | number of persons |
| R | retention time |
| V | volume |
| q | flow rate |
| f | sizing factor |
| r | primary sludge build up rates in litres per person per year |
| BOD | biological oxygen demand |
| COD | chemical oxygen demand |

LIST OF ABBREVIATIONS

| STED Septic Tank Effluent Drainage | STED | Septic Tank Effluent Drainage |
|------------------------------------|------|-------------------------------|
|------------------------------------|------|-------------------------------|

VIP Ventilated Improved Pit Latrine

LOFLOS A Low Flow, On-site Sanitation System using a low volume flush, an

anaerobic digester to treat the flow, and a soakaway. These are generally

sold as package units

THE DETERMINATION OF SLUDGE BUILD-UP RATES IN SEPTIC TANKS, BIOLOGICAL DIGESTERS AND PIT LATRINES IN SOUTH AFRICA

1. BACKGROUND

Efforts to meet the need for basic sanitation facilities in rapidly growing, low income communities have led to an awareness of the necessity to look at alternative means of providing sanitation services. Pit latrines, on-site digesters and septic tank systems are increasingly being installed as appropriate alternatives to water-borne sanitation.

As with any other system, one of the factors that influences the total cost of these systems is the cost of operation and maintenance. In the case of on-site systems this cost is mainly dependent on the life-span of the pit or tank or the emptying frequency thereof.

The bacterial digestion process on which the operation of these systems is based, does not break down one hundred per cent of the tank contents and therefore a layer of partially digested sludge accumulates in the digestion chambers of all three systems. In practice this means that a digestion tank fills up over time and has to be emptied at one stage or another or, if this is not possible, it has to be abandoned. Part of the optimization of the designs of these systems is to design the digestion chamber for a specific economic emptying cycle. For the purpose of optimised design of on-site sanitation systems it is necessary to have a proper indication of the rate of sludge accumulation in a specific type of system operating under certain circumstances.

The CSIR has recently been involved in two research projects that included a study of, in the first instance, the filling rate of a public pit latrine in Constantia Park, Pretoria, and secondly the sludge accumulation rates in biological digesters installed in the township Marselle, near Boesmansriviermond in the Eastern Cape. Both these investigations provided reasons to doubt the figures that are commonly used for digestion chamber design. Although this type of study has been done elsewhere for septic tanks and approximated figures have been published for pit latrines, there is still uncertainty surrounding the performance of biological digesters and as the above mentioned projects showed, there are numerous factors affecting the performance of on-site systems that have not yet been quantified. It is possible that some of these factors pertain to local customs and conditions and therefore the discrepancy between the results of an American study and local phenomena could be ascribed to the effect of local conditions such as diet and cleansing habits.

Other considerations that have brought the importance of sludge build-up rates to the fore are:

- The emergence of the LOFLOS Systems in South Africa and the whole debate on the design principles pertaining to these systems, have highlighted the question of sludge build-up.
- In the past, domestic septic tanks were generally built so excessively big in relation to their loadings that sludge build-up never became a problem. It was only at institutions that accommodated a large number of people (hotels, hostels) or from which large volumes of waste water originated (abattoirs, industries) where regular desludging had to take place.
- The prefabricated tanks of all the commercially available on-site digesters and septic tanks are sized optimally, i.e. as small as possible to minimise costs. Sludge accumulation therefore plays a more important role.
- Since the periodic emptying of any tank based sanitation system has an important bearing on the operation costs thereof, it is important to be able to predict beforehand what the emptying frequency of a particular system would be under certain circumstances.
- Some manufacturers of prefabricated septic tanks and on-site digesters claim very long periods between emptying intervals for their systems, and no substantial evidence is available to contradict these claims. The users of these systems eventually have to bear the brunt of the false claims. It is important to establish proper design figures to give decision makers a factual basis for decisions about systems.
- Septic tank effluent drainage systems (STED systems), also known as solids free or small bore sewer systems are also gaining popularity in South Africa. Sludge build-up in the interceptor tanks is an important factor in the design and operation of these systems.

2. AIMS OF THE PROJECT

- To identify the factors that could possibly affect the sludge accumulation in specific on-site sanitation systems.
- To select a representative sample of on-site systems for the investigation of the factors affecting sludge build-up.
- To determine the sludge build-up rates of a representative sample of specific onsite sanitation systems.

- To quantify the factors affecting the sludge build-up in the named systems.
- To combine the relevant factors in a relation whereby the sludge build-up rate for a specific type of system can be predicted for design purposes.

3. LITERATURE SURVEY

The following information on the topic of sludge build-up has been obtained through the literature survey:

Hill, F.G. & Ackers, G.L. 1954. <u>Principles of design for small domestic-sewage-treatment works</u>. Design and operation of septic tanks, World Health organisation Monograph Series, no. 18: 31-57.

A tank cleaned once a year will require 96 ℓ of scum and sludge storage space per head, whereas by doubling the storage space the frequency of cleansing could be reduced to once in four and a half years.

Small rural plants: The provision to be made for the storage of sludge and scum for a six month period should be $68,2 \ \ell$ per head.

The sludge and scum storage space required for a 12-month de-sludging period amounts to an average of 96 ℓ per head and if allowance is made for seeding sludge, the capacity required for a 12-month interval should be 116 ℓ per head.

• Drews, R.J.L.C. 1985. A guide to the use of septic tank systems in South Africa. CSIR: Pretoria.

This publication concentrates on conventional septic tanks with 9 litre flush toilets. Bath and other grey water is also drained to the septic tank.

Table 1: Rate of sludge and scum accumulation

| Years of service | Sludge & scum accumulation (ℓ/person) |
|------------------|--|
| 1 | 95 |
| 2 | 120 |
| 4 | 175 |
| 6 | 235 |
| 8 | 305 |
| 10 | 385 |

The data in Table 1 is represented graphically in Figure 1. A linear regression analysis was carried out on the data. The slope of the straight regression line is the sludge build-up rate. The rate is 32 l/p/yr or 0.09 l/p/d.

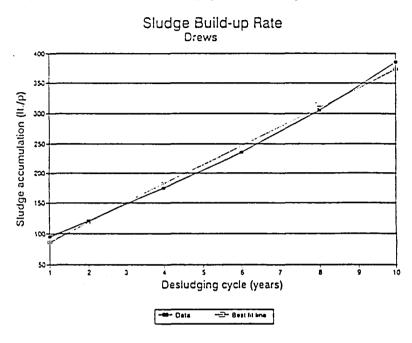


Figure 1. Sludge build-up rates (Drews)

• Weibel, S.R., Straub, C.P. and Thomas, J.R. 1949. <u>Studies on household</u> sewage <u>disposal systems</u>. US Dept. of Health: Cincinnati, Ohio.

The sludge build-up rate derived from measurements on 205 American septic tanks is **22** *l*/**p/yr** or **0.06** *l*/**p/d**. Flushing volumes would typically be in the 13-18 litre range.

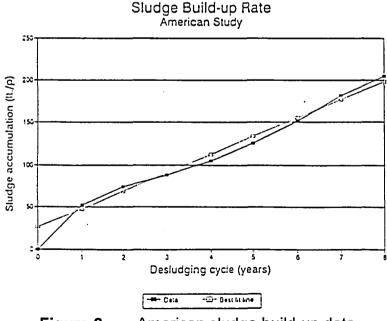


Figure 2. American sludge build-up data

• ENSIC. 1982. <u>Septic tank and septic systems</u>. Environmental sanitation reviews, no. 7/8.

In the Indian code the sludge accumulation rate is taken as 77 $\ell/p/yr$ (0,21 $\ell/p/day$).

• Sewards, G.J., Fimmel, R.J. 1982. <u>On-site wastewater disposal in Perth</u>. Metropolitan Water Authority: Perth.

Table 2: Results of an Australian survey.

| Item | | Accumulati | ion in l/p/yr | |
|--------|--------|------------|---------------|---------------|
| | Range | Average | Median | 90 Percentile |
| Sludge | 8 - 58 | 28 | 27 | 48 |
| Scum | 0 - 45 | 19 | 18 | 32 |

• Sahle, H. 1988. <u>Applicability of small bore gravity sewers in Addis Ababa, Ethiopia</u>. Asian Institute of Technology: Bangkok.

This model combines the effects of temperature, type of cleansing materials used and the source of the waste water. The figure for sludge build-up, given as litres per person per year, is acquired by choosing values for "f" and "r" from Tables 3 and 4 below and then multiplying these two factors, to obtain the sludge build-up rate.

Table 3: Values of sizing factor "f" for stated desludging intervals and temperatures (Sahle 1988:12).

| desludging interval (years) | more than 20 °C throughout year | more than 10 °C throughout year | less than 10 °C during winter time |
|-----------------------------------|------------------------------------|------------------------------------|---------------------------------------|
| 1 | 1.3 | 1.5 | 2.5 |
| 2 | 1.0 | 1.15 | 1.5 |
| 3 | 1.0 | 1.0 | 1.27 |
| 4 | 1.0 | 1.0 | 1.15 |
| 5 | 1.0 | 1.0 | 1.06 |
| 6+ | 1.0 | 1.0 | 1.0 |

Table 4: Primary sludge build-up rates "r" in litres per person per year (Sahle 1988:13).

| materials used for anal cleansing | water closet or latrine wastes only | household sullage in addition to waste |
|-----------------------------------|--|--|
| water, soft paper | 25 | 40 |
| leaves, hard paper | 40 | 55 |
| sand, stone, earth | 55 | 70 |

Brandes, M. 1978. <u>Accumulation rate and characteristics of septic tank</u> <u>sludge and septage.</u> Journal Water Pollution Control Federation, 936 - 943

Extracts of data from this Canadian study is given in Table 5.

Table 5: Results of a Canadian study.

| Location of septic tank | Hawkestone farm | Orilla Hospital house | Whitby experimental | |
|----------------------------------|-------------------|---|---|--|
| nature of treated waste water | toilet wastewater | toilet, bathroom and kitchen wastewater | toilet, bathroom, kitchen, laundry wastewater | |
| No. of users | 3 | 11 | 28 | |
| Detention time (d) | ~9.7 | ~2.4 | ~1.9 | |
| Sludge build-up rate (ℓ/p/d) | 0.18 | 0.22 | 0.29 | |

• Franceys, R., Pickford, J., Reed, R. 1992. <u>A guide to the development of on-site sanitation</u>. World Health Organisation : Geneva.

According to this publication, very little information is available on sludge accumulation rates. Factors with the biggest effect on accumulation rates in pit latrines are whether decomposition takes place above or below the water table and the type of anal cleaning material used. The suggested rates are shown in table 6. It is also advised that local sludge accumulation rates be measured before designing latrines. In the absence of local data the figures in the table below can be used. Note that the authors consider them to be on the high side.

Table 6: Suggested sludge accumulation rates (Franceys) (Litres per person per year)

| | Accumulation rate |
|--|-------------------|
| Wastes retained in water where degradable anal cleaning materials are used | 40 |
| Wastes retained in water where non-degradable anal cleaning materials are used | 60 |
| Waste retained in dry conditions where degradable anal cleaning materials are used | 60 |
| Waste retained in dry conditions where non- degradable anal cleaning materials are used | 90 |

3.1 Summary of sludge build-up rates

The sludge build-up rates in the literature are given in different units. To aid comparison the results of the literature survey are summarized below with the sludge build-up rates given in litres/person/day, which is the unit used throughout the rest of this document. A year is assumed to comprise 365 days.

Note that the results of the Canadian study in table 5 above indicate that the addition of kitchen and laundry chemicals results in an increase in the sludge build up rate. This may indicate that these chemicals inhibit bacterial activity. However, kitchen wastes result in a greater biological loading and this may also contribute to the higher sludge build up rate.

Table 7: Summary of sludge build-up data in septic tanks reported in literature.

| Reference | Country | Type of sanitation system | Sludge build-up rate |
|-----------------------------|--------------|---------------------------|----------------------------|
| | | | (ℓ/p/d) |
| Hill & Ackers, 1954 | not specific | Septic tank | 0.26 |
| Drews, 1985 | South Africa | Septic tank | 0.09 |
| Wiebel, Stub & Thomas, 1949 | USA | Septic tank | 0.06 |
| ENSIC, 1982 | India | Septic tank | 0.21 |
| Sewards & Fimmel, 1982 | Australia | | 0.08 |
| Brandes, 1978 | Canada | Septic tank | 0.18 |

Note that all the above studies were for conventional septic tank systems with flush toilets. Franceys suggests figures to use for on-site systems other than septic tanks and this information is quoted in Table 6. The literature survey revealed that very little research on sludge accumulation rates has been undertaken. Most of the literature quotes figures in general use with no attempt to measure local rates.

4. FACTORS AFFECTING SLUDGE BUILD-UP

The following factors were considered to affect the sludge build-up rate in digesters and pit latrines.

4.1 Number of users

The amount of waste entering a pit or digester is obviously dependant on the number of people making use of the sanitation system. If the sanitation system involves flushing, more users means more water going through the system, which will shorten the retention time.

4.2 Anal cleansing material

Two kinds of anal cleansing paper are most popular with the users of on-site sanitation systems, namely conventional toilet paper or newsprint paper. The newsprint paper consists mostly of old newspapers, although magazines are also used.

Newsprint is generally tougher than toilet paper and is therefore expected to take longer to break down than toilet paper. In addition, the ink on these papers may adversely affect bacteria.

4.3 Diet

The nature of the diet will affect the BOD and COD introduced into a pit or digester.

The biological digestion processes are also affected by the proportions of carbon, nitrogen and phosphorous. The optimum BOD:N:P ratio is 100:10:1. These proportions are determined by the protein and carbohydrate intake of the user of the sanitation system. Imbalances in the ratio can lead to an inefficient digestion process and therefore higher sludge build-up rates.

The information required in respect of the diet is therefore the proportion of carbohydrates and proteins. Data obtained from residents, when asked about their diets, was unfortunately not sufficiently reliable to provide a good indicator.

4.4 Soil conditions

Pit Latrines: Soil conditions will have a greater effect on the sludge build-up rate in pit latrines than in digesters. This is so because pit latrines are normally unlined and the flow of water to and from the sludge depends on the permeability of the soil. Soil samples, on which permeability tests were carried out, were taken from each of the pit latrine sites.

Digester systems: For a properly functioning digester with unblocked soakaway, soil will have no effect on sludge build-up rate as the digestion process is isolated from the soil by the tank. The soakaway may fail due to an insufficiently permeable soil, however. As this state of affairs does not represent a functioning sanitation system, soil was considered to have no effect on digesters.

4.5 Seasonal effects

The research team expected to find pronounced seasonal effects on the sludge buildup rates in pit latrines due to effects of rain on the moisture content in the pits. However, no evidence was found to support this theory in the pit latrines monitored.

4.6 Retention time

The retention time (also called detention time) is a measure of the average length of time that the wastewater remains in a digester tank before flowing out of the tank. It depends on the volume of the digester tank and the flow rate of the influent.

```
R = V/q

where R = retention time (days)

V = tank volume (litres)

q = influent flow rate (litres/day)
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The Canadian research reported in Table 5 seems to indicate that the longer the retention time, the lower the sludge build-up rate.

4.7 Characteristics of influent

The influent may consist of toilet waste only or may include other wastes such as bathroom, kitchen or laundry water. This can be expected to have an effect on the sludge build-up rate. Chemicals in kitchen and bathroom wastes may inhibit bacterial activity in the tank and cause the sludge build-up rate to increase.

4.8 Chemicals used for toilet cleaning

Since some of the commercially available products can harm the biological activity in the tank, the use of these products could be expected to increase the sludge build up rate in the system. However, if these substances are used in small quantities the effect is likely to be minimal. This was evidenced during the project where tanks were seen to be functioning satisfactorily, but on speaking to the residents it was found that these products were used regularly for toilet cleaning.

4.9 Temperature

The temperature in the system can have a marked effect on the sludge build up rate. For every 10 °C rise in temperature the rate of metabolism is expected to increase by a factor of 1,8.

5. METHODS AND EQUIPMENT

5.1 Monitoring of digesters

Figure 3 shows the sludge sampler which was designed to determine the sludge and scum depths in septic tanks and biological digesters. This device is used to core the contents of the tank in order to get an indication of the particular stratification.

The brass rod with the conical plastic stopper is lowered into the tank through the access opening until it reaches the bottom. The clear perspex tube is then inserted into the tank with the brass rod passing through the centre of the tube. The plastic cone will guide the perspex tube onto the rubber sealing ring. The tube is then tightened against the sealing ring by the stopper screwed on at the top of the tube.

This method was found to give a good indication of the sludge and supernatant liquor layers in the tanks. The sludge is of a viscous nature and the plastic cone easily penetrated the sludge layer. The clarity of the supernatant liquor was a good indication of the efficiency of digestion taking place in the tank. The clearer the supernatant liquor, the more efficient the digestion process.

The tanks in Warden, Umbumbulu and Ivory Park were cored using this technique on a cycle of about once every 10 weeks.

5.2 Monitoring of pit latrines

Pit latrines are dry sanitation systems and a different monitoring approach was necessary in this instance. The sludge level was determined by measuring the vertical distance between a fixed datum (top of toilet seat) and the sludge. A steel measuring tape attached to a steel weight was used as the measuring apparatus. The change in the vertical distance then indicates the change in sludge volume.

As the waste material is deposited in the pit from one point, a mound was formed in the pit. Depending on the moisture of the sludge, the steepness of the mound varied, being very steep in the dry season and flatter in the rainy season. The vertical distance to the top of the toilet seat was therefore measured from a point half-way between the top and the base of the mound. The pit latrines were measured about once every 10 weeks.

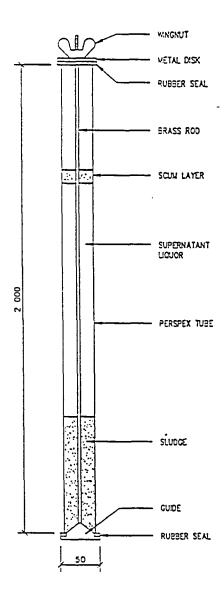


Figure 3. Sludge sampler used for determining sludge and scum depth (Not to scale, dimensions in mm)

6. SYSTEMS MONITORED FOR THIS STUDY

The following on-site sanitation systems were monitored for this study:

- System A: Interceptor tanks in a STED system at Marselle township near Boesmansriviermond.
- System B: Public VIP latrines at Constantia Park, Pretoria.

- System C: Loflo digesters at Umbumbulu near Durban.
- System D: Septic tanks at Warden in the Free State.
- System E: VIP latrines at Soshanguve north of Pretoria.
- System F: Loflo digesters at Ivory Park near Midrand.

These systems are described below:

6.1 System A: Interceptor Tanks at Marselle

Marselle is situated near Boesmansriviermond in the Eastern Cape. Houses are generally of concrete block construction. A STED system was installed by the Cape Provincial Administration in November 1989. Two types of toilets systems, a flush and a non-flush system, were installed in the township. Both systems used a 1750 ℓ polyethylene interceptor tank. The flush system consisted of a conventional P-trap pan with a 5 litre flush. A wash trough with a tap, which also drained into the interceptor tank, was installed on the outside of the toilet hut. Compared with the situation at Warden, this was a low income area with less water passing through the tanks. The non-flush system consists of a ceramic pan without a P-trap that discharges into a long radius bend connected to the interceptor tank below the water level. The water in the long radius bend forms a rough water seal. Waste is either flushed into the tank by pouring a bucket of water into the pan or a plunger with a flexible rod is used to push the waste into the tank. The STED sewers are drained to a series of ponds some distance away from the settlement. Visits to the ponds led to the conclusion that they are much bigger than necessary and also that they are seldom, if ever, maintained.

These systems were monitored by the CSIR, the Cape Provincial Administration and the manufacturer of the interceptor tank. The tank is the same shape as those monitored at Ivory Park and shown in figure 5, the only difference being that the Marselle tanks have a volume of 1 750 litres while those at Ivory Park are 1 000 litres.

During the course of this project the CPA decided to replace the non-flush systems at Marselle with flush toilets. The ceramic pans were removed and replaced with plastic pans and cisterns. The long radius bends were blocked off and conventional connections made to the tank. This effectively converted these systems to the same as the other installations at Marselle. The research team spoke to the engineers at the CPA about the reasons for the alterations to the "dry" systems and this interview is attached in Appendix III. In summary, they found that most of the problems associated with the STED system at Marselle were associated with the "dry" systems. Residents did not like using the plunger to push the waste into the tank. In addition it appeared as if the tanks were never filled with water. The other problems relate to a lack of funds for maintenance at Marselle.

6.2 System B: VIP latrines at Constantia Park

Pit latrines were erected at a bus stop in Constantia Park, a suburb of Pretoria, in 1986 and monitored for a period of 6 years. The latrines were the only public sanitation facility in the area of the bus stop. They were constructed of brick to a standard design as indicated in NBRI information sheets. (X/BOU 2-17: The ventilated improved pit latrine. M A Heap)

Separate pits were constructed for men and women, with volumes of 4,45 m³ and 3,04 m³ respectively. Counters were attached to the gates leading to the toilets and urinals so that the exact number of users could be determined. Toilet rolls were contained in special dispensers so that the exact number of toilet rolls used could be determined.

6.3 System C: Biological digesters at Umbumbulu

The digester system used in Umbumbulu consists of a tipping-tray pedestal installed inside the house and a 1 000 litre digester tank made from glass-reinforced plastic (GRP). Waste enters the tank at the centre through a curved funnel-shaped GRP pipe. This pipe is attached to the tank by means of a flexible coupling to allow for differential movement. Effluent is drawn from the centre of the tank via the integral outlet. The tank is covered with a full opening lid. The pedestal is designed to use one litre of water per flush. A cross-sectional drawing of a tank is shown in Figure 4. The tank is drained to an on-site soakaway. Kitchen waste bypasses the tank and goes directly to the soakaway.

Most of the houses were constructed of brick or concrete blocks by Time Housing. Loans were provided to the residents through employee housing schemes. In discussions with residents it was found that most of them were told by agents when they bought their houses that the sanitation system would be replaced within a short space of time with a waterborne sanitation system. The fact that this has not yet happened has given rise to a general non-acceptance of the existing systems.

10 tanks were monitored for this study. A screw cap at the centre of the full opening lid was provided for inserting the sludge monitoring tube.

The tanks at the following houses were monitored:

| House No. | Tank No. | House No. |
|-----------|------------------------------|--------------------------------------|
| C924 | 6 | C905 |
| C925 | 7 | C840 |
| C926 | 8 | C839 |
| C908 | 9 | C834 |
| C907 | 10 | C833 |
| | C924 C925 C926 C908 | C924 6 C925 7 C926 8 C908 9 |

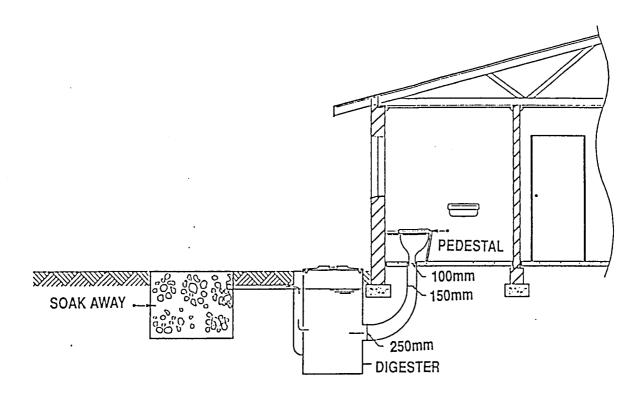


Figure 4. Biological digesters at Umbumbulu.

6.4 System D: Septic tanks at Warden

Warden is a small farming community in the Free State. The houses in Warden used to be served by conservancy tanks which were emptied twice a week. The sanitation system was upgraded in the mid 1990s by connecting the tanks to a STED system. The existing conservancy tanks, with volumes of between 3 500 and 4 000 litres, were not replaced. An outlet T-piece was installed in each tank. The STED sewers drain to the same ponds that were used for the treatment of conservancy tank waste. In discussions with the Town Clerk it was found that the STED system is working very well. The only problems are with the tanks – they are very old, and many of the cover slabs are broken or badly cracked.

6.5 System E: Pit latrines at Soshanguve

The pit latrines at Soshanguve were excavated using a 1m diameter auger. The pits therefore have a round cross-section with a depth of about 2,50 m. The pits were covered with precast concrete slabs, on top of which prefabricated corrugated iron superstructures were installed. The pedestals in the toilets are made from wood. These

latrines are not considered to be acceptable. They do not stop the breeding of flies and they tend to smell. The superstructures get very hot in the sun and reverse venting occurs. The superstructures also have large openings between the walls and the roof, resulting in a lot of light falling on the pedestal; as a result, flies are not attracted to the ventpipe where they would be trapped by the flyscreen. The pedestals are made of chipboard which soaks up urine spillage, leading to odours.

Although these are not good examples of VIP latrines, the shortcomings would not affect the sludge accumulation rate.

6.6 System F: Biological digesters at Ivory Park

Ivory Park was one of the first townships in Gauteng to be developed on a site and service basis. Because there is only one standpipe per 20 stands there is no fully waterborne sanitation. Each 200 m² stand has one toilet. All of these toilets are on-site sanitation systems. Some of these have very small tanks (~35 litres) and others are anaerobic digesters with 1 000 litre tanks. It was decided that only the 1 000 litre tanks would be monitored. All the toilets are housed in prefabricated corrugated iron huts.

A cross-section of the larger digester tanks monitored in Ivory Park is shown in Figure 5. The cylindrical tank has a conical top section. The tank is 1,20 m in diameter when measured across the bottom surface, with a height of 1,35 m. A T-shaped effluent outlet pipe is positioned 1,0 m above the bottom surface of the tank, inside a cone-shaped baffle protruding 630 mm into the tank. This results in a 1 000 litre liquid capacity and 250 litre free air space.

Sludge readings were taken by inserting the sludge monitoring tube in the manhole at the top of the tank, which is normally covered with a concrete filled lid.

Because the total depth (bottom of tank to outflow level) is 1,0 m the sum of the sludge and fluid level should not exceed this distance. A total depth greater than 1,0 m indicates that either the soak away or the overflow pipe is blocked, resulting in unsatisfactory, and potentially hazardous, operation of the tank.

The digesters were installed in November 1990.

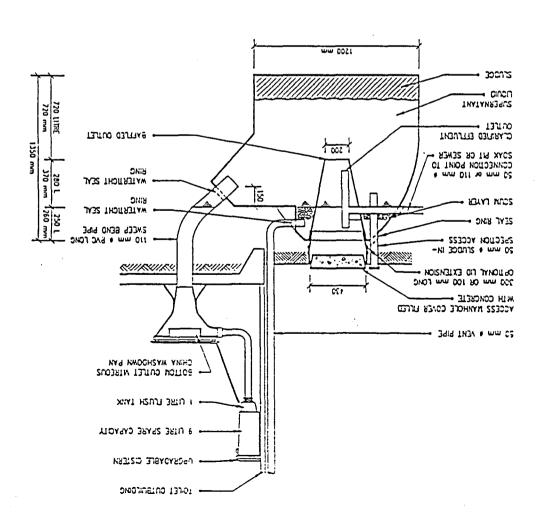


Figure 5. Cross section of digester tank at Ivory Park

7. RESULTS OF INVESTIGATION

7.1 Sludge monitoring

The sludge build-up rates determined by direct measurement are given below. Units are litres/person/day.

Table 8: Sludge build-up rates as determined on site

| Description | Range | Mean | # of measurements |
|-----------------------------------|---------------|-------|----------------------|
| Marselle: Non-flush systems | 0.087 - 0.247 | 0.178 | 26 |
| Marselle: Flush systems | 0.074 - 0.140 | 0.101 | 24 |
| Umbumbulu: Tipping-tray digesters | 0.020 - 0.193 | 0.074 | 117 |
| Ivory Park: Anaerobic digesters | 0.055 - 0.123 | 0.083 | 15 |
| Warden: Septic tanks | 0.030 - 0.370 | 0.149 | 140 |
| Soshanguve: VIP latrines | 0.036 - 0.093 | 0.066 | 102 |

Constantia park: Public pit latrines:

Toilet for males: average usage: 765 users per month.

filling rate: 0,06 //person/day.

Toilet for females: average usage: 494 users per month.

filling rate: 0,80 //person/day.

7.2 Soil investigations

Soil investigations were only undertaken for on-site sanitation systems where the effluent is discharged to a soil percolation system. The soil property which has the greatest affect on water absorption and soakaway performance is permeability. This was determined in the laboratory using a constant-head permeameter.

Soil samples were taken at the sites listed in Table 8. Constantia Park and Soshanguve sites both have VIP latrines and so the soil permeability can be expected to have a direct influence on the sludge build up rates. Umbumbulu and Ivory Park are Loflo digester systems with on-site soakaways. The results of the soil investigation are summarized in Table 8:

Table 9: Soil permeabilities

| Sample | Laboratory permeability k (cm/s) |
|----------------------|----------------------------------|
| Umbumbulu, Sample 1 | 4.19 × 10⁻⁵ |
| Umbumbulu, Sample 2 | 1.02 × 10⁻⁴ |
| Ivory Park, Sample 1 | 4.31 × 10 ⁻⁴ |
| Ivory Park, Sample 2 | 5.64 × 10 ⁻⁴ |
| Ivory Park, Sample 3 | 5.19 × 10 ⁻⁴ |
| Soshanguve, Sample 1 | 7.41 × 10⁴ |
| Soshanguve, Sample 2 | 1.32 × 10⁴ |
| Soshanguve, Sample 3 | 1.75 × 10 ⁻⁴ |

7.3 Socio-economic surveys

Socio-economic surveys were conducted to correlate income levels to the sludge buildup rate. Income level can usually give an indication of diet composition.

7.3.1 Ivory Park

Ivory Park is situated in close proximity to the industrial areas of Midrand and Kempton Park. A relatively large number residents (73%) therefore have full time employment.

7.3.2 Soshanguve

Soshanguve is situated to the north of Pretoria. Although unemployment is relatively high the pit latrines are situated in an area with conventional housing and it seems as if the residents are in regular employment.

7.3.3 Umbumbulu

The area monitored is part of a housing scheme in Folweni. Most of the houses were built by Time Housing for SA Breweries. The owners of these houses are mostly employed at the breweries.

7.4 User Perceptions

As part of the monitoring programme, the users of the toilet systems were asked their opinions on the use of their on-site sanitation systems. Except for the STED system in Warden, most users were negative towards their respective toilets. This is mainly because their demands for full waterborne sewerage had not yet been met and the expectations that this would still be provided. The most common complaints and perceptions are listed below:

- Smell and flies: Virtually every user of the VIP latrines in Soshanguve complained about smell and flies. The strongest complaints related to especially large concentrations of flies during summer months. Associated with these complaints were concerns about the health of occupants.
- Fear of children falling into pits or tanks: Understandably, these fears were expressed mostly by users with young children.
- Poor workmanship: A lot of complaints were received about the flushing mechanisms of the systems installed in Umbumbulu. The complaints were normally in connection with poor quality washers. Other examples of poor workmanship were pedestals not installed horizontally, causing water to leak out of the tipping tray and failed tipping tray mechanisms.
- Responsibilities not clearly understood: Users did not understand that they
 were responsible for looking after their toilets. They also did not fully understand
 the basic maintenance requirements of the systems. This is probably due to
 inadequate user training.

7.5 General observations during monitoring

- The septic tanks at Warden usually had well defined separation between the sludge and liquid layers. The liquid layer was very clear.
- There was usually a well defined separation with the LOFLOS systems but the liquid layer was generally much less clear than in the septic tanks.
- There was very little scum accumulation in all the systems monitored.
- Building a cheap VIP latrine is a waste of time and money. The latrines at Soshanguve do nothing to stop the spread of disease carried by flies and they provide an appalling level of service to the user.
- In most of the areas monitored, the residents had been promised that their systems would shortly be upgraded to waterborne sanitation. These unrealistic promises have resulted in dissatisfaction with the present systems.

8. PROBLEMS EXPERIENCED DURING MONITORING PROGRAMME

Some problems occurred in the capture of data. This was mostly due to communication problems

- 1. Improper emptying of tanks: It was often found that tanks showed relatively high levels of sludge after they had supposedly been emptied. It was therefore suspected that the tanks were not being entirely emptied. This suspicion was confirmed by the responsible foreman in Warden, who said that about 200 mm of sludge is normally left behind in the tanks after pumping. In discussion with maintenance personnel at other townships, it transpired that often only the liquids are removed from the tanks, and very little sludge. The emptying is done by contractors with minimal supervision from the local authority. Furthermore, the tanks are usually left empty instead of being filled with water.
- 2. **Users not home:** Very often users were not home when the survey sites were visited so that information on matters such as the number of users, diet and anal cleansing material could not be updated. In these cases it was assumed, for purposes of the analysis, that the variable had not changed since the last survey for which information was available. Where a change in the number of users occurred, the average number of users was used for the analysis.
- 3. **Sample size:** Due to cost constraints, the sample sizes chosen were too small. According to CSIR statisticians, a rule of thumb is to choose a sample size of 10 times the number of variables considered.
- 4. **Inadequate data on tank emptying:** In many cases the users were unable to specify exactly or even roughly when the tanks were last emptied, and the local authority records were also unreliable.
- 5. **Political instability:** Most of the monitoring work was carried out in politically sensitive areas over a time of political transition. Consequently, toilet systems could not always be monitored at the required intervals.

9. DISCUSSION AND CONCLUSIONS

9.1 Sludge build-up rates

The sludge build-up in litres/person was plotted against time and these graphs are reproduced in Appendix II. A line of best fit was plotted on these graphs and the slope of the line measured, giving the build-up rate in litres/person/day. In this process events such as emptying of the tanks was taken into account. Outlying points that

could not be explained were excluded. Table 10 below indicates the total number of measurements taken during this project and the number that could be used to determine the sludge build-up rates.

Table 10: Measurements used to determine build-up rates

| Place | # of sites | # of visits | Total measurements | Measurements used |
|------------|------------|-------------|-----------------------|----------------------|
| Umbumbulu | 10 | 16 | 160 | 117 |
| Warden | 14 | 13 | 182 | 140 |
| Soshanguve | 11 | 14 | 154 | 102 |
| Ivory Park | 9 | 11 | 99 | 15 |

As can be seen from the table, very few measurements from Ivory Park could be used. The depth of sludge in the tanks showed considerable variation. The tanks were emptied periodically and no record of this emptying could be obtained from the township office or the residents. The emptying was often not done properly and it is believed that, in most cases, only some of the liquid was pumped out and very little, if any, of the sludge. It is also believed that the tanks were seldom filled with water after emptying.

9.2 Accumulation rate versus number of people

When the average accumulation rates are plotted against the number of people resident on the property, no evidence of correlation can be found. This could mean that the number of people contributing waste to the system does not affect the sludge build-up rate.

9.3 Scum accumulation

Several design manuals for septic tanks quote figures for accumulation of scum and thus require designers to allow a volume for the storage of scum. This study, however, revealed that whereas there is a need to design for a floating layer of scum, there is no need to provide additional volume for storage of accumulated scum. The normal practice of placing a T-piece on the outlet to prevent the scum from leaving the tank is sufficient. On tanks with a small surface area the T-piece should be extended higher than normal to allow for the rise in liquid level when a large volume of liquid enters the tank.

9.4 Recommended design criteria

1. The following values are recommended for sludge accumulation in South Africa:

VIP latrines 0.07 litres/person/day Septic tanks and Loflo systems 0.08 litres/person/day

2. No provision needs to be made for scum accumulation. A T-piece should be placed on the outlet to prevent floating scum from leaving the tank.

10. GENERAL RECOMMENDATIONS

- 1. **User education:** In many cases toilet systems do not function satisfactorily due to user ignorance. Once a toilet is installed, the correct operating procedures should be explained to the user, in his or her own language, so that there are no misunderstandings.
- 2. **Correct installation:** Responsibility for correct installation of toilet systems should be clearly defined and the quality of workmanship monitored on site.
- 3. **Minimum tank size:** Tanks for Loflo digester systems where water is supplied from standpipes should not be less than 1000 litres in volume. If the tanks are to be connected to a STED sewer system then consideration should be given to installing a larger tank, for example 1750 litres. The larger tank is suggested because of the greater volume of water passing through the tank and the impact of kitchen wastes on the rate of sludge build up.
- 4. **Minimum pit size:** VIP latrines need to be properly designed and constructed. This has a cost implication and would probably mean that one would need to design the latrine for a longer life cycle before emptying is required. It would therefore be best to construct the pit as large as possible, given site and cost constraints. It should be borne in mind, however, that if it is the intention for a VIP latrine be emptied by means of a vacuum tanker, then the depth of the pit should be limited (2 m is suggested as a maximum in this case).

11. RECOMMENDATIONS FOR FURTHER RESEARCH

- Optimum size for Loflo sanitation systems: Research into this aspect will require
 a detailed study of the processes inside the tank. During the course of this
 project, it was seen that the large tanks at Warden operate very well; this leads
 one to question if the 1 000 litre volume currently used for Loflo systems is
 adequate.
- Low-maintenance sanitation systems: It was found that many local authorities have insufficient funds or staff to carry out maintenance tasks properly. Research and information dissemination on low-maintenance systems are required.

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| DATE DAYS CUMULAT. DAYS | 07/22/93 0 0 | 09/27/93 68 68 | 12/13/93 77 145 | 02/16/94 65 210 | 04/14/94 58 268 | 06/22/94 69 337 | 10/24/94 124 461 | 12/06/94 43 504 | 01/26/95 50 554 | 04/11/95 75 629 | 06/12/95 62 691 | 08/30/95 79 770 | 10/24/95 55 825 |
|--|--------------------------|--|---|--|--|---|--|--|--|---|--|--|---|
| 7DE LAAN NO. 6 NO. OF USERS | ADULTS 5 | CHILDREN 0 | | AREA: | 4.3 | | | | | | | | |
| SCUM FLUID SLUDGE SLUDGE VOL. (L/P) ST-RATE LT-RATE XLT-RATE | 0 1335 200 172 | | 5 1678 165 141.9 -0.1116883 -0.2075862 | 10 1360 145 124.7 -0.2646154 -0.2252381 | 5 1340 180 154.8 0.5189655 0.104878 | 15 1325 190 163.4 0.1246377 | 5 1305 210 180.6 0.13871 0.13368 0.22271 | 5 1320 200 172 -0.2 | 10 1340 180 154.8 -0.344 -0.27742 | 5 1370 170 146.2 -0.11467 -0.20476 | 10 1350 190 163.4 0.27742 0.06277 | 10 1165 180 154.8 -0.10886 | 10 1290 215 184.9 0.54727 0.16045 0.19745 |
| 7DE LAAN NO 8 NO. OF USERS | ADULTS (| CHILDREN 0 | | AREA: | 3.86 | | | | | | | | |
| SCUM FLUID SLUDGE SLUDGE VOL. (L/P) ST-RATE LT-RATE XLT-RATE | 0 1200 70 135.1 | 0 1235 85 164.05 0.4257353 | 0 1350 75 144.75 -0.2506494 0.0665517 | | 0 1165 60 115.8 -0.6655172 -0.2353659 | 0 1255 70 135.1 0.2797101 | 0 1185 105 202.65 0.54476 0.45 0.19223 | 10 1335 155 299.15 2.24419 | 5 1365 155 299.15 0 1.03763 | 5 1390 160 308.8 0.12867 0.63185 | 5 1450 180 347.4 0.62258 0.35219 | 10 1495 200 386 0.48861 | 15 1535 180 347.4 -0.70182 0 0.19694 |

| DATE DAYS CUMULAT. DAYS | 07/22/93 0 0 | 09/27/93 68 68 | 12/13/93 77 145 | 02/16/94 65 210 | 04/14/94 58 268 | 06/22/94 69 337 | 10/24/94 124 461 | 12/06/94 43 504 | 01/26/95 50 554 | 04/11/95 75 629 | 06/12/95 62 691 | 08/30/95 79 770 | 10/24/95 55 825 |
|------------------------------------|--------------------|----------------------|-----------------------|-----------------------|-----------------------|-----------------------|------------------------|-----------------------|-----------------------|-----------------------|-----------------------|-----------------------|-----------------------|
| 7DE LAAN NO 10 | ADULTS | CHILDREN | | AREA: | 2.88 | | | | | | | | |
| NO. OF USERS | 2 | 0 | | | | | | | | | | | |
| SCUM | 0 | 0 | 0 | 10 | 15 | 40 | 10 | 25 | 25 | 0 | 0 | 5 | 5 |
| FLUID | 840 | 950 | 1220 | 1175 | 1245 | 1200 | 790 | 810 | 870 | 765 | 750 | 660 | 750 |
| SLUDGE | 180 | 90 | 70 | 120 | 155 | 250 | 200 | 170 | 135 | 145 | 75 | 260 | 240 |
| SLUDGE VOL. (L/P) | 259.2 | 129.6 | 100.8 | 172.8 | 223.2 | 360 | 288 | 244.8 | 194.4 | 208.8 | 108 | 374.4 | 345.6 |
| ST-RATE | | -1.9058824 | -0.374026 | 1.1076923 | 0.8689655 | 1.9826087 | -0.58065 | -1.00465 | -1.008 | 0.192 | -1.62581 | 3.37215 | -0.52364 |
| LT-RATE | | | -1.0924138 | | 0.995122 | | 0.33575 | | -1.00645 | | -0.63066 | | 1.77313 |
| XLT-RATE | | | | -0.4114286 | | | 0.45896 | | | -0.47143 | | | 0.69796 |
| 7DE LAAN NO 12 NO. OF USERS | ADULTS | CHILDREN 0 | | AREA: | 2.86 | | | | | | | | |
| THO OF COLING | | | | | | | | | | | | | |
| SCUM | 0 | 5 | 10 | 20 | 20 | 0 | 25 | 15 | 15 | 10 | 10 | 25 | 50 |
| FLUID | 1360 | 1515 | 1320 | 1560 | 1485 | 1290 | 1255 | 1275 | 1275 | 1250 | 1245 | 1195 | 1205 |
| SLUDGE | 180 | 150 | 150 | 220 | 195 | 170 | 175 | 210 | 200 | 160 | 170 | 210 | 200 |
| SLUDGE VOL. (L/P) | 128.7 | 107.25 | 107.25 | 157.3 | 139.425 | 121.55 | 125.125 | 150.15 | 143 | 114.4 | 121.55 | 150.15 | 143 |
| ST-RATE | | -0.3154412 | 0 | 0.77 | -0.3081897 | -0.259058 | 0.02883 | 0.58198 | -0.143 | -0.38133 | 0.11532 | 0.36203 | -0.13 |
| LT-RATE | | | -0.147931 | | 0.2615854 | | -0.07409 | | 0.1922 | | -0.15657 | | 0.16007 |
| XLT-RATE | | | | 0.1361905 | | | -0.12819 | | | -0.06384 | | | 0.14592 |

| DATE | 07/22/93 | 09/27/93 | 12/13/93 | 02/16/94 | 04/14/94 | 06/22/94 | 10/24/94 | 12/06/94 | 01/26/95 | 04/11/95 | 06/12/95 | 08/30/95 | 10/24/95 |
|-----------------------|----------|-----------|-----------|------------|-----------|------------|----------|----------|----------|----------|----------|----------|----------|
| DAYS | 0 | 68 | 77 | 65 | 58 | 69 | 124 | 43 | 50 | 75 | 62 | 79 | 55 |
| CUMULAT. DAYS | 0 | 68 | 145 | 210 | 268 | 337 | 461 | 504 | 554 | 629 | 691 | 770 | 825 |
| | | | | | | | | | | | | | |
| | | | | | | | | | | | | | |
| CORNER 7DE + PARK | | CHILDREN | | AREA: | 3.66 | | | | | | | | |
| NO. OF USERS | 2 | 0 | | | | | | | | | | | |
| SCUM | 0 | 0 | 10 | 5 | 5 | 0 | 0 | 0 | 5 | 10 | 5 | 0 | 10 |
| FLUID | 0 | 945 | 945 | 1130 | 845 | 910 | 800 | 805 | 850 | 900 | 860 | 765 | 800 |
| | 0 | 95 | 130 | 100 | 180 | 120 | 225 | 220 | 180 | 135 | 180 | 250 | 210 |
| SLUDGE CLUDGE | 0 | | | | | | | | | | | | |
| SLUDGE VOL. (L/P) | U | 173.85 | 237.9 | 183 | 329.4 | 219.6 | 411.75 | 402.6 | 329.4 | 247.05 | 329.4 | 457.5 | 384.3 |
| ST-RATE | | 2.5566176 | | -0.8446154 | 2.5241379 | -1.5913043 | | -0.21279 | -1.464 | -1.098 | 1.32823 | 1.02152 | -1.33091 |
| LT-RATE | | | 1.6406897 | | 0.7439024 | | 0.42668 | | -0.88548 | | 0 | | 0.4097 |
| XLT-RATE | | | | 0.8714286 | | | 0.91135 | | | -0.98036 | | | 0.70026 |
| | | | | | | | | | | | | | |
| | | | | | | | | | | | | | |
| | | | | | | | | | | | | | |
| CORNER 8STE + PARK(21 | ADULTS | CHILDREN | | AREA: | 2.89 | | | | | | | | |
| NO. OF USERS | 3 | 0 | | | | | | | | | | | |
| | | | | | | | | | | | | | |
| SCUM | 0 | 0 | 0 | 0 | 0 | 0 | 5 | 0 | 0 | 0 | 0 | 0 | 0 |
| FLUID | 880 | 1000 | 1290 | 1160 | 780 | 875 | 740 | 770 | 800 | 815 | 550 | 765 | 750 |
| SLUDGE | 145 | 175 | 175 | 165 | 180 | 140 | 180 | 185 | 220 | 130 | 120 | 200 | 230 |
| SLUDGE VOL. (L/P) | 139.6833 | 168.58333 | 168.58333 | 158.95 | 173.4 | 134.86667 | 173.4 | 178.217 | 211.933 | 125.233 | 115.6 | 192.667 | 221.567 |
| ST-RATE | | 0.425 | 0 | -0.1482051 | 0.2491379 | -0.5584541 | 0.31075 | 0.11202 | 0.67433 | -1.156 | -0.15538 | 0.97553 | 0.52545 |
| LT-RATE | | | 0.1993103 | | 0.0391599 | | 0 | | 0.41434 | | -0.70316 | | 0.7908 |
| XLT-RATE | | | | 0.091746 | | | 0.05757 | | | -0.28671 | | | 0.4915 |

| DATE | 07/22/93 | 09/27/93 | 12/13/93 | 02/16/94 | 04/14/94 | | | | | | | 08/30/95 | |
|-------------------|----------|------------|------------|------------|------------|-----------|----------|----------|----------|----------|----------|----------|----------|
| DAYS | 0 | 68 | 77 | 65 | 58 | 69 | 124 | 43 | 50 | 75 | 62 | 79 | 55 |
| CUMULAT. DAYS | 0 | 68 | 145 | 210 | 268 | 337 | 461 | 504 | 554 | 629 | 691 | 770 | 825 |
| 8STE LAAN NO 15 | ADULTS | CHILDREN | | AREA: | 2.56 | | | | | | | | |
| NO. OF USERS | 2 | 0 | | | | | | | | | | | |
| SCUM | 0 | 0 | . 0 | 0 | 0 | 0 | 5 | 5 | 5 | _ | 0 | 20 | 10 |
| FLUID | 1185 | 1185 | 1285 | 1400 | 1440 | 1310 | 1085 | 1145 | 1120 | | 1120 | 1105 | 1100 |
| SLUDGE | 100 | 125 | 120 | 80 | 115 | 120 | 250 | 135 | 155 | 150 | 120 | 170 | 200 |
| SLUDGE VOL. (L/P) | 128 | 160 | 153.6 | 102.4 | 147.2 | 153.6 | 320 | 172.8 | 198.4 | 192 | 153.6 | 217.6 | 256 |
| ST-RATE | | 0.4705882 | -0.0831169 | -0.7876923 | 0.7724138 | 0.0927536 | 1.34194 | -3.42326 | 0.512 | -0.08533 | -0.61935 | 0.81013 | 0.69818 |
| LT-RATE | | | 0.1765517 | | -0.0520325 | | 0.89534 | | -1.30753 | | -0.32701 | | 0.76418 |
| XLT-RATE | | | | -0.1219048 | | | 0.86693 | | | -0.7619 | | | 0.32653 |
| | | | | | | | | | | | | | |
| 8STE LAAN NO 13 | ADULTS | CHILDREN | | AREA: | 3.82 | | | | | | | | |
| NO. OF USERS | 3 | 0 | | | | | | | | | | | |
| SCUM | 0 | 0 | 0 | 5 | 5 | 0 | 5 | 0 | 0 | 0 | 0 | 0 | 0 |
| FLUID | 865 | 1260 | 1280 | 1280 | 340 | 790 | 840 | 830 | 870 | 845 | 865 | 780 | 760 |
| SLUDGE | 270 | 155 | 180 | 130 | 160 | 200 | 170 | 170 | 160 | 170 | 120 | 220 | 180 |
| SLUDGE VOL. (L/P) | 343.8 | 197.36667 | 229.2 | 165.53333 | 203.73333 | 254.66667 | 216.467 | 216.467 | 203.733 | 216.467 | 152.8 | 280.133 | 229.2 |
| ST-RATE | | -2.1534314 | 0.4134199 | -0.9794872 | 0.6586207 | 0.7381643 | -0.30806 | | -0.25467 | 0.16978 | -1.02688 | 1.61181 | -0.92606 |
| LT-RATE | | | -0.7903448 | | -0.2070461 | | 0.06598 | | -0.13692 | | -0.37178 | | 0.57015 |
| XLT-RATE | | | | -0.8488889 | | | 0.20292 | | | 0 | | | 0.06497 |
| | | | | | | | | | | | | | |

SLUDGE MONITORING AT WARDEN

| DATE DAYS CUMULAT. DAYS | 07/22/93 0 0 | 09/27/93 68 68 | 12/13/93 77 145 | 02/16/94 65 210 | 04/14/94 58 268 | 06/22/94 69 337 | 10/24/94 124 461 | 12/06/94 43 504 | 01/26/95 50 554 | 04/11/95 75 629 | 06/12/95 62 691 | 08/30/95 79 770 | 10/24/95 55 825 |
|---------------------------------|--------------------|----------------------|-----------------------|-----------------------|-----------------------|-----------------------|------------------------|-----------------------|-----------------------|-----------------------|-----------------------|-----------------------|-----------------------|
| 8STE LAAN NO 11 NO. OF USERS | ADULTS 4 | CHILDREN 0 | | AREA: | 3.6 | | | | | | | | |
| Tro. of obline | · | v | | | | | | | | | | | |
| SCUM | 5 | 7 | 0 | 5 | 5 | 5 | 10 | 10 | 5 | 10 | 10 | 15 | 10 |
| FLUID | 1170 | 1580 | 1680 | 1090 | 1105 | 1100 | 1070 | 1080 | 1040 | 1040 | 1030 | 908 | 1000 |
| SLUDGE | 120 | 120 | 110 | 110 | 185 | 200 | 210 | 170 | 235 | 210 | 235 | 245 | 210 |
| SLUDGE VOL. (L/P) | 108 | 108 | 99 | 99 | 166.5 | 180 | 189 | 153 | 211.5 | 189 | 211.5 | 220.5 | 189 |
| ST-RATE | | 0 | -0.1168831 | 0 | 1.1637931 | 0.1956522 | 0.07258 | -0.83721 | 1.17 | -0.3 | 0.3629 | 0.11392 | -0.57273 |
| LT-RATE | | | -0.062069 | | 0.5487805 | | 0.11658 | | 0.24194 | | 0 | | -0.16791 |
| XLT-RATE | | | | -0.0428571 | | | 0.35857 | | | 0 | | | 0 |
| | | | | | | | | | | | | | |
| 8STE LAAN NO 7 | ADULTS | CHILDREN | J | AREA: | 3.024 | | | | | | | | |
| NO. OF USERS | 1 | 0 | | | 5.02. | | | | | | | | |
| SCUM | 0 | 5 | 0 | 5 | 0 | 0 | 10 | 0 | 0 | 0 | 2 | 0 | 0 |
| FLUID | 900 | 1050 | 1145 | 1335 | 1345 | 1330 | 800 | 800 | 790 | 845 | 790 | 810 | 725 |
| SLUDGE | 110 | 140 | 135 | 120 | 115 | 135 | 190 | 165 | 150 | 150 | 170 | 170 | 230 |
| SLUDGE VOL. (L/P) | 332.64 | 423.36 | 408.24 | 362.88 | 347.76 | 408.24 | 574.56 | 498.96 | 453.6 | 453.6 | 514.08 | 514.08 | 695.52 |
| ST-RATE | | 1.3341176 | -0.1963636 | -0.6978462 | -0.2606897 | 0.8765217 | 1.34129 | -1.75814 | -0.9072 | 0 | 0.97548 | 0 | 3.29891 |
| LT-RATE | | | 0.5213793 | | -0.4917073 | | 1.17513 | | -1.30065 | | 0.44146 | | 1.35403 |
| XLT-RATE | | | | 0.144 | | | 0.84335 | | | -0.72 | | | 1.23429 |

SLUDGE MONITORING AT WARDEN

| DATE | 07/22/93 | 09/27/93 | 12/13/93 | 02/16/94 | 04/14/94 | | 10/24/94 | | | | | | = |
|-------------------|----------|-----------|------------|------------|-----------|------------|----------|----------|----------|----------|----------|---------|----------|
| DAYS | 0 | 68 | 77 | 65 | 58 | 69 | 124 | 43 | 50 | 75 | 62 | 79 | 55 |
| CUMULAT. DAYS | 0 | 68 | 145 | 210 | 268 | 337 | 461 | 504 | 554 | 629 | 691 | 770 | 825 |
| 8STE LAAN NO 3 | ADULTS | CHILDREN | Ī | AREA: | 3.483 | | | | | | | | |
| NO. OF USERS | 2 | 0 | | | | | | | | | | | |
| SCUM | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 |
| FLUID | 1030 | 1010 | 1010 | 1030 | 1105 | 1015 | 975 | 995 | 1040 | 980 | 1000 | 955 | 1000 |
| SLUDGE | 35 | 65 | 60 | 50 | 65 | 75 | 100 | 80 | 75 | 85 | 60 | 90 | 85 |
| SLUDGE VOL. (L/P) | 60.9525 | 113.1975 | 104.49 | 87.075 | 113.1975 | 130.6125 | 174.15 | 139.32 | 130.613 | 148.028 | 104.49 | 156.735 | 148.028 |
| ST-RATE | | 0.7683088 | -0.1130844 | -0.2679231 | 0.4503879 | 0.2523913 | 0.35111 | -0.81 | -0.17415 | 0.2322 | -0.70222 | 0.66133 | -0.15832 |
| LT-RATE | | | 0.3002586 | | 0.0707927 | | 0.31582 | | -0.46815 | | -0.19068 | | 0.32491 |
| XLT-RATE | | | | 0.1243929 | | | 0.34691 | | | -0.15549 | | | 0 |
| | | | | | | | | | | | | | |
| BOARD. HOUSE | ADULTS | CHILDREN | | AREA: | 18 | | | | | | | | |
| NO. OF USERS | 8 | 30 | | | | | | | | | | | |
| SCUM | 0 | 50 | 45 | 20 | 20 | 0 | 30 | 25 | 0 | 10 | 25 | 50 | 15 |
| FLUID | 0 | 470 | 380 | 300 | 200 | 310 | 400 | 380 | 320 | 350 | 390 | 375 | 400 |
| SLUDGE | 0 | 100 | 105 | 180 | 210 | 140 | 60 | 55 | 155 | 150 | 80 | 100 | 90 |
| SLUDGE VOL. (L/P) | 0 | 47.368421 | 49.736842 | 85.263158 | 99.473684 | 66.315789 | 28.4211 | 26.0526 | 73.4211 | 71.0526 | 37.8947 | 47.3684 | 42.6316 |
| ST-RATE | | 0.6965944 | 0.0307587 | 0.5465587 | 0.2450091 | -0.4805492 | -0.3056 | -0.05508 | 0.94737 | -0.03158 | -0.5348 | 0.11992 | -0.08612 |
| LT-RATE | | | 0.3430127 | | 0.4043646 | | -0.36815 | | 0.48387 | | -0.25932 | | 0.03535 |
| XLT-RATE | | | | 0.406015 | | | -0.22646 | | | 0.25376 | | | -0.14501 |

SLUDGE MONITORING AT WARDEN

| DATE DAYS CUMULAT. DAYS | 07/22/93 0 0 | 09/27/93 68 68 | 12/13/93 77 145 | 02/16/94 65 210 | 04/14/94 58 268 | 06/22/94 69 337 | 10/24/94 124 461 | 12/06/94 43 504 | 01/26/95 50 554 | 04/11/95 75 629 | 06/12/95 62 691 | 08/30/95 79 770 | 10/24/95 55 825 |
|--|-------------------------|--------------------------------------|---|--|--|---------------------------------|--|--------------------------------------|--|---|---|--------------------------------------|--|
| 7DE LAAN 20 NO. OF USERS | ADULTS | CHILDREN 0 | | AREA: | 4.4 | | | | | | | | |
| SCUM FLUID SLUDGE SLUDGE VOL. (L/P) ST-RATE LT-RATE XLT-RATE | 0 1075 90 132 | 0 1445 150 220 1.2941176 | 0 975 130 190.66667 -0.3809524 0.4045977 | 0 1195 145 212.66667 0.3384615 0.384127 | 0 400 120 176 -0.6321839 -0.1192412 | | 5 1115 125 183.333 0.2957 0.038 -0.11687 | 0 1120 120 176 -0.17054 | 0 970 125 183.333 0.14667 0 | 5 1130 100 146.667 -0.48889 -0.21825 | 5 1085 150 220 1.1828 0.26764 | 10 1010 240 352 1.67089 | 5 1010 200 293.333 -1.06667 0.54726 0.7483 |
| 7DE LAAN NO 23 NO. OF USERS | ADULTS | CHILDREN 0 | Ţ | AREA: | 3.465 | | | | | | | | |
| SCUM FLUID SLUDGE SLUDGE VOL. (L/P) ST-RATE LT-RATE XLT-RATE | 0 1000 60 69.3 | 0 1155 80 92.4 0.3397059 | 0 1200 70 80.85 -0.15 0.0796552 | 0 1220 75 86.625 0.0888462 | 0 1170 110 127.05 0.6969828 0.3756098 | 0 1145 110 127.05 0 | 0 1190 90 103.95 -0.18629 -0.11969 0.06902 | 0 1170 95 109.725 0.1343 | 0 1145 100 115.5 0.1155 0.12419 | 0 1155 120 138.6 0.308 | 0 1170 110 127.05 -0.18629 0.08431 | 0 1155 140 161.7 0.43861 | 0 1230 140 161.7 0 0.25858 0.11786 |

| BIOTAG DIAMETER AREA | 1.0m 0.785 | | | | | | | | | | | | | | | |
|-------------------------|---------------|----------------|-----------|----------------|----------------|----------------|----------------|----------------|-----------------|-----------------|----------------|----------|----------|----------------|----------------|----------------|
| DATE DAYS | 11/12/92 0 | 01/13/93 62 | 03/17/93 | 05/18/93 63 | 07/21/93 64 | 09/28/93 69 | 12/15/93 78 | 02/18/94 65 | 06/24/94 126 | 10/26/94 124 | 12/07/94 42 | 02/16/95 | 04/11/95 | 06/14/95 64 | 09/01/95 79 | 10/26/95 55 |
| CUMULAT. DAYS | 0 | 62 | 125 | 188 | 252 | 321 | 399 | 464 | 590 | 714 | 756 | 827 | 881 | 945 | 1024 | 1079 |
| C924 | | CHILDREN | | AREA: | 0.785 | | | | | | | | | | | |
| NO. OF USERS | 5 | 2 | | | | | | | | | | | | | | |
| SCUM | 30 | 20 | 5 | 10 | 60 | 200 | 130 | 220 | 310 | - | - | 15 | 5 | 50 | 50 | 100 |
| FLUID | 870 | 1050 | 920 | 925 | 980 | 900 | 870 | 1085 | 1190 | - | - | 1215 | 1155 | 1105 | 1100 | 1000 |
| SLUDGE | 380 | 110 | 330 | 360 | 210 | 250 | 260 | 185 | 90 | - | - | 50 | 105 | 150 | 150 | 270 |
| SLUDGE VOLUME (L) | 298.3 | 86.35 | 259.05 | 282.6 | 164.85 | 196.25 | 204.1 | 145.225 | 70.65 | 0 | 0 | 39.25 | 82.425 | 117.75 | 117.75 | 211.95 |
| ST-RATE | | -0.488364 | 0.39161 | 0.0534014 | -0.262835 | 0.0650104 | 0.0143773 | -0.129396 | -0.084552 | -0.0814 | 0 | 0.07897 | 0.11422 | 0.07885 | 0 | 0.24468 |
| LT-RATE | | | -0.044857 | | -0.105962 | | 0.0381438 | | -0.099813 | | -0.0608 | | 0.0942 | | 0.03529 | |
| XLT-RATE | | | | -0.01193 | | | -0.053148 | | | -0.0926 | | | 0.07051 | | | 0.09345 |
| SLUDGE VOL. (L/P) | 42.6143 | 12.335714 | | | | | | 20.746429 | 10.092857 | 0 | - | 5.60714 | 11.775 | 16.8214 | 16.8214 | 30.2786 |
| CUMLAT. RATE | | 0.1989631 | 0.2960571 | 0.2147416 | 0.0934524 | 0.0873387 | 0.0730755 | 0.0447121 | 0.0171065 | 0 | 0 | 0.00678 | 0.01337 | 0.0178 | 0.01643 | 0.02806 |
| C015 | A DI II T | CHILDREN | | AREA: | 0.785 | | | | | | | | | | | |
| C925 NO. OF USERS | ADULI 3 | CHILDREN 1 | | AKEA: | 0.783 | | | | | | | | | | | |
| NO. OF USERS | 3 | 1 | | | | | | | | | | | | | | |
| SCUM | 0 | 0 | 0 | 0 | 5 | 0 | 10 | 20 | 40 | 0 | 0 | 0 | 0 | 10 | 10 | 20 |
| FLUID | 1130 | 400 | 900 | 955 | 870 | 670 | 940 | 600 | 500 | 450 | 305 | 1220 | 1165 | 1110 | 1000 | 915 |
| SLUDGE | 150 | 250 | 385 | 290 | 400 | 520 | 300 | 670 | 760 | 800 | 965 | 80 | 125 | 200 | 300 | 360 |
| SLUDGE VOLUME (L) | 117.75 | 196.25 | 302.225 | 227.65 | 314 | 408.2 | 235.5 | 525.95 | 596.6 | 628 | 757.525 | 62.8 | 98.125 | 157 | 235.5 | 282.6 |
| ST-RATE | | 0.3165323 | 0.4205357 | -0.295933 | | 0.3413043 | | 1.1171154 | | 0.06331 | 0.77098 | -2.44621 | | 0.22998 | 0.24842 | 0.21409 |
| LT-RATE | | | 0.36895 | | 0.0231791 | | -0.133503 | | 0.472644 | | 0.24236 | | -1.3188 | | 0.24017 | |
| XLT-RATE | | | | 0.1461436 | | | 0.0093009 | | | 0.31151 | | | -0.7932 | | | 0.23292 |
| SLUDGE VOL. (L/P) | 29.4375 | 49.0625 | 75.55625 | 56.9125 | 78.5 | 102.05 | 58.875 | 131.4875 | 149.15 | 157 | 189.381 | 15.7 | | 39.25 | 58.875 | 70.65 |
| CUMLAT. RATE | | 0.7913306 | 0.60445 | 0.3027261 | 0.3115079 | 0.3179128 | 0.1475564 | 0.2833782 | 0.2527966 | 0.21989 | 0.2505 | 0.01898 | 0.02784 | 0.04153 | 0.0575 | 0.06548 |

| BIOTAG DIAMETER AREA | 1.0m 0.785 | | | | | | | | | | | | | | | |
|-------------------------|---------------|-----------|-----------|-----------|-----------|-----------|-----------|-------------|-----------|----------|----------|----------|----------|----------|----------|----------|
| DATE | 11/12/92 | 01/13/93 | 03/17/93 | 05/18/93 | 07/21/93 | 09/28/93 | 12/15/93 | 02/18/94 | 06/24/94 | 10/26/94 | 12/07/94 | 02/16/95 | 04/11/95 | 06/14/95 | 09/01/95 | 10/26/95 |
| DAYS | 0 | 62 | 63 | 63 | 64 | 69 | 78 | 65 | 126 | 124 | 42 | 71 | 54 | 64 | 79 | 55 |
| CUMULAT. DAYS | 0 | 62 | 125 | 188 | 252 | 321 | 399 | 464 | 590 | 714 | 756 | 827 | 881 | 945 | 1024 | 1079 |
| C834 | ADULT | CHILDREN | | AREA: | 0.785 | !! TURNED | INTO SEPT | TIC TANK !! | | | | | | | | |
| NO. OF USERS | 5 | 3 | | | | | | | | | | | | | | |
| SCUM | 0 | 5 | 25 | 5 | 20 | 40 | 25 | 0 | 5 | 5 | 10 | 5 | 10 | 10 | 20 | 10 |
| FLUID | 1200 | 1180 | 1130 | 1170 | 1140 | 1120 | 1010 | 1220 | 1120 | 1100 | 1100 | 1240 | 1220 | 1190 | 1190 | 1120 |
| SLUDGE | 80 | 100 | 175 | 130 | 150 | 170 | 250 | 80 | 140 | 180 | 180 | 40 | 55 | 95 | 75 | 80 |
| SLUDGE VOLUME (L) | 62.8 | 78.5 | 137.375 | 102.05 | 117.75 | 133.45 | 196.25 | 62.8 | 109.9 | 141.3 | 141.3 | 31.4 | 43.175 | 74.575 | 58.875 | 62.8 |
| ST-RATE | | 0.0316532 | 0.1168155 | -0.070089 | 0.0306641 | 0.028442 | 0.100641 | -0.256635 | 0.0467262 | 0.03165 | | -0.19349 | | 0.06133 | -0.02484 | 0.00892 |
| LT-RATE | | | 0.074575 | | -0.019316 | | 0.0667517 | | -0.056512 | | 0.02364 | | -0.0981 | | 0.04574 | |
| XLT-RATE | | | | 0.0260971 | | | 0.0558057 | | | -0.0218 | | | -0.0734 | | | 0.01239 |
| SLUDGE VOL. (L/P) | 7.85 | | 17.171875 | 12.75625 | 14.71875 | 16.68125 | 24.53125 | 7.85 | 13.7375 | | | | | | 7.35938 | 7.85 |
| CUMLAT. RATE | | 0.1582661 | 0.137375 | 0.0678524 | 0.0584077 | 0.0519665 | 0.0614818 | 0.0169181 | 0.0232839 | 0.02474 | 0.02336 | 0.00475 | 0.00613 | 0.00986 | 0.00719 | 0.00728 |
| C833 | ADULT | CHILDREN | | AREA: | 0.785 | | | | | | | | | | | |
| NO. OF USERS | 2 | 4 | | | | | | | | | | | | | | |
| SCUM | 80 | 0 | 40 | 50 | 260 | 230 | 325 | 280 | 350 | - | _ | 0 | 0 | 0 | 30 | 25 |
| FLUID | 1050 | 0 | 935 | 1020 | 1030 | 840 | 775 | 1070 | | - | - | 1010 | 900 | 855 | 865 | 630 |
| SLUDGE | 120 | 0 | 300 | 240 | 200 | 300 | 110 | 170 | | - | - | 170 | 330 | 370 | 370 | 530 |
| SLUDGE VOLUME (L) | 94.2 | 0 | 235.5 | 188.4 | 157 | 235.5 | 86.35 | 133.45 | 0 | 0 | 0 | 133.45 | 259.05 | 290.45 | 290.45 | 416.05 |
| ST-RATE | | -0.253226 | 0.6230159 | -0.124603 | -0.081771 | 0.1896135 | -0.318697 | 0.1207692 | -0.176521 | 0 | 0 | 0.31326 | 0.38765 | 0.08177 | 0 | 0.38061 |
| LT-RATE | | | 0.1884 | | -0.103018 | | -0.080102 | | -0.075349 | | 0 | | 0.3454 | | 0.0366 | |
| XLT-RATE | | | | 0.0835106 | | | -0.080608 | | | -0.0457 | | | 0.25853 | | | 0.13215 |
| SLUDGE VOL. (L/P) | 15.7 | 0 | 39.25 | 31.4 | 26.166667 | | 14.391667 | | 0 | 0 | 0 | | | 48.4083 | 48.4083 | 69.3417 |
| CUMLAT. RATE | | 0 | 0.314 | 0.1670213 | 0.103836 | 0.1222741 | 0.0360693 | 0.0479346 | 0 | 0 | 0 | 0.02689 | 0.04901 | 0.05123 | 0.04727 | 0.06426 |

| BIOTAG DIAMETER AREA | 1.0m 0.785 | | | | | | | | | | | | | | | |
|-------------------------|---------------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|---|----------|----------|----------|----------|----------|----------|----------|
| DATE | 11/12/92 | 01/13/93 | 03/17/93 | 05/18/93 | 07/21/93 | 09/28/93 | 12/15/93 | 02/18/94 | 06/24/94 | 10/26/94 | 12/07/94 | 02/16/95 | 04/11/95 | 06/14/95 | 09/01/95 | 10/26/95 |
| DAYS | 0 | 62 | 63 | 63 | 64 | 69 | 78 | 65 | 126 | 124 | 42 | 71 | 54 | 64 | 79 | 55 |
| CUMULAT. DAYS | 0 | 62 | 125 | 188 | 252 | 321 | 399 | 464 | 590 | 714 | 756 | 827 | 881 | 945 | 1024 | 1079 |
| COMOLATI. DATIO | Ū | 02 | 120 | 100 | 202 | | 2,, | | • | ,,,, | ,,,, | 027 | 001 | , 10 | 1021 | 10// |
| C840 | ADULT | CHILDREN | | AREA: | 0.785 | | | | | | | | | | | |
| NO. OF USERS | 5 | 4 | | | | | | | | | | | | | | |
| SCUM | 0 | 0 | 0 | 0 | 5 | 0 | 0 | 0 | 0 | 15 | 25 | 0 | 0 | 10 | 10 | 10 |
| FLUID | 1255 | 0 | 1140 | 1095 | 1020 | 990 | 1000 | 1025 | 775 | 720 | 800 | 800 | 845 | 855 | 795 | 985 |
| SLUDGE | 25 | 0 | 145 | 205 | 270 | 255 | 255 | 230 | 350 | 560 | 480 | 430 | 300 | 350 | 395 | 400 |
| SLUDGE VOLUME (L) | 19.625 | 0 | 113.825 | 160.925 | 211.95 | 200.175 | 200.175 | 180.55 | 274.75 | 439.6 | 376.8 | 337.55 | 235.5 | 274.75 | 310.075 | 314 |
| ST-RATE | | -0.03517 | 0.2007496 | 0.0830688 | 0.0885851 | -0.018961 | 0 | -0.033547 | 0.0830688 | 0.14772 | -0.1661 | -0.06142 | -0.21 | 0.06814 | 0.04968 | 0.00793 |
| LT-RATE | | | 0.0837333 | | 0.0858486 | | -0.0089 | | 0.0433828 | | 0.06831 | | -0.1256 | | 0.05794 | |
| XLT-RATE | | | | 0.0835106 | | | 0.0206688 | | | 0.08445 | | | -0.1358 | | | 0.04405 |
| SLUDGE VOL. (L/P) | 2.18056 | 0 | 12.647222 | 17.880556 | 23.55 | 22.241667 | 22.241667 | 20.061111 | 30.527778 | 48.8444 | 41.8667 | 37.5056 | 26.1667 | 30.5278 | 34.4528 | 34.8889 |
| CUMLAT. RATE | | 0 | 0.1011778 | 0.0951093 | 0.0934524 | 0.0692887 | 0.0557435 | 0.0432352 | 0.051742 | 0.06841 | 0.05538 | 0.04535 | 0.0297 | 0.0323 | 0.03365 | 0.03233 |
| | | | | | 0.505 | HODIGON | | | | | | | | | | |
| C839 | | CHILDREN | | AREA: !!! | 0.785 | HORIZON | TANK !!! | | | | | | | | | |
| NO. OF USERS | 3 | 3 | | | | | | | | | | | | • | | |
| SCUM | 0 | - | 40 | 5 | 10 | 7 | 15 | 20 | 40 | 50 | 85 | 25 | 0 | 50 | 50 | 50 |
| FLUID | 640 | 575 | 640 | 570 | 545 | 550 | 555 | 550 | 500 | 400 | 385 | 370 | 350 | 360 | 290 | 335 |
| SLUDGE | 0 | | 0 | 175 | 189 | 200 | 190 | 200 | 215 | 330 | 350 | 380 | 400 | 370 | 420 | 370 |
| SLUDGE VOLUME (L) | 0 | 78.5 | 0 | 137.375 | 148.365 | 157 | 149.15 | 157 | 168.775 | 259.05 | 274.75 | 298.3 | 314 | 290.45 | 329.7 | 290.45 |
| ST-RATE | | 0.2110215 | -0.207672 | 0.3634259 | 0.0286198 | 0.0208575 | | 0.0201282 | 0.0155754 | 0.12134 | 0.0623 | 0.05528 | 0.04846 | -0.06133 | 0.08281 | -0.11894 |
| LT-RATE | | | 0 | | 0.1947047 | | 0.00089 | | 0.0171248 | | 0.1064 | | 0.05233 | | 0.0183 | |
| XLT-RATE | | | | 0.1217863 | | | 0.0093009 | | | 0.05815 | | | 0.05484 | | | -0.01982 |
| SLUDGE VOL. (L/P) | 0 | 13.083333 | 0 | 22.895833 | 24.7275 | 26.166667 | 24.858333 | 26.166667 | 28.129167 | 43.175 | 45.7917 | 49.7167 | | 48.4083 | 54.95 | 48.4083 |
| CUMLAT. RATE | | 0.2110215 | 0 | 0.1217863 | 0.098125 | 0.0815161 | 0.0623016 | 0.0563937 | 0.0476766 | 0.06047 | 0.06057 | 0.06012 | 0.0594 | 0.05123 | 0.05366 | 0.04486 |

| BIOTAG DIAMETER AREA | 1.0m 0.785 | | | | | | | | | | | | | | | |
|---|------------------------------|--|-----------------------|---|---|--|--|--|---|------------------------|---|---|---|--|-------------------------------|------------------------|
| DATE DAYS CUMULAT. DAYS | 11/12/92 0 0 | 01/13/93 62 62 | 03/17/93 63 125 | 05/18/93 63 188 | 07/21/93 64 252 | 09/28/93 69 321 | 12/15/93 78 399 | 02/18/94 65 464 | 06/24/94 126 590 | 10/26/94 124 714 | 12/07/94 42 756 | 02/16/95 71 827 | 04/11/95 54 881 | 06/14/95 64 945 | 09/01/95 79 1024 | 10/26/95 55 1079 |
| C907 NO. OF USERS | ADULT 2.5 | CHILDREN 3 | | AREA: | 0.785 | | | | | | | | | | | |
| SCUM FLUID SLUDGE SLUDGE VOLUME (L) ST-RATE LT-RATE XLT-RATE SLUDGE VOL. (L/P) CUMLAT. RATE | | 1200 90 70.65 0.2071848 12.845455 0.2071848 | 0.0799273 | 35 1145 160 125.6 0.2038961 0.12147 22.836364 0.12147 AREA: | 20 1120 180 141.3 0.0446023 0.123622 25.690909 0.1019481 | 31.4 | 0.0776747 0.0676433 37.109091 | | 35 1210 100 78.5 0.0453102 -0.119562 14.272727 0.0241911 | | | | 5 1215 110 86.35 0.21145 -0.1656 0.02564 15.7 0.01782 | 0 1135 180 141.3 0.15611 25.6909 0.02719 | 0.09937 0.12476 33.5409 | |
| NO. OF USERS SCUM FLUID SLUDGE SLUDGE VOLUME (L) ST-RATE LT-RATE XLT-RATE SLUDGE VOL. (L/P) CUMLAT. RATE | 4 0 1080 200 157 | 5 950 300 235.5 0.3165323 58.875 0.9495968 | -0.1099 25.5125 | 10 990 300 235.5 0.5295635 0.1043883 58.875 0.3131649 | 5 980 300 235.5 0 0.2626969 58.875 0.233631 | 0 920 350 274.75 0.1422101 68.6875 0.2139798 | 830 435 341.475 0.2138622 0.1802296 0.1255628 85.36875 | 5 765 520 408.2 0.2566346 102.05 0.2199353 | 0 890 360 282.6 -0.249206 -0.077062 70.65 0.1197458 | 0.0405 98.125 | 15 845 390 306.15 -0.514 0.03547 76.5375 0.10124 | 30 810 460 361.1 0.19349 90.275 0.10916 | 20 785 500 392.5 0.14537 0.1727 0 98.125 0.11138 | 82.425 | 78.5 | |

| BIOTAG DIAMETER AREA | 1.0m 0.785 | | | | | | | | | | | | | | | |
|---|---------------------------|---|--|---|--|---|---|--|---|--|--|---|--|---|---|--|
| DATE DAYS CUMULAT. DAYS | 11/12/92 0 0 | 01/13/93 62 62 | 03/17/93 63 125 | 05/18/93 63 188 | 07/21/93 64 252 | 09/28/93 69 321 | 12/15/93 78 399 | 02/18/94 65 464 | 06/24/94 126 590 | 10/26/94 124 714 | 12/07/94 42 756 | 02/16/95 71 827 | 04/11/95 54 881 | 06/14/95 64 945 | 09/01/95 79 1024 | 10/26/95 55 1079 |
| C926 NO. OF USERS | ADULT 4 | CHILDREN 0 | | AREA: | 0.785 | | | | | | | | | | | |
| SCUM FLUID SLUDGE SLUDGE VOLUME (L) ST-RATE LT-RATE XLT-RATE SLUDGE VOL. (L/P) CUMLAT. RATE | 0 1120 160 125.6 | 980 250 196.25 0.284879 49.0625 0.7913306 | 0 1030 190 149.15 -0.186905 0.0471 37.2875 0.2983 | 0 985 255 200.175 0.2024802 0.0991689 50.04375 0.2661902 | 0.1468012 55.93125 | 2 890 340 266.9 0.1564312 66.725 0.207866 | 5 970 250 196.25 -0.226442 -0.046726 -0.00465 49.0625 0.1229637 | 5 870 345 270.825 0.2868269 67.70625 0.1459186 | 0.1323909 0.1849476 84.3875 | | 0 790 425 333.625 0.14018 -0.0059 83.4063 0.11033 | 0 1220 10 7.85 -1.1471 1.9625 0.00237 | 0 1160 80 62.8 0.2544 -0.5417 -0.3702 15.7 0.01782 | 0 1120 120 94.2 0.12266 23.55 0.02492 | | 5 1000 230 180.55 0.37466 0.14867 45.1375 0.04183 |
| C908 NO. OF USERS | ADULT 3 | CHILDREN 2 | | AREA: | 0.785 | | | | | | | | | | | |
| SCUM FLUID SLUDGE SLUDGE VOLUME (L) ST-RATE LT-RATE XLT-RATE SLUDGE VOL. (L/P) CUMLAT. RATE | 0 0 0 0 | 5 1110 170 133.45 0.4304839 26.69 0.4304839 | 0 1055 225 176.625 0.1370635 0.2826 35.325 0.2826 | 0 1005 240 188.4 0.037381 0.2004255 37.68 0.2004255 | 5 1000 270 211.95 0.0735938 0.0556299 42.39 0.1682143 | 47.1 | 0 930 350 274.75 0.100641 0.0854422 0.0818483 54.95 0.1377193 | 54.95 | 0 790 500 392.5 0.1869048 0.1232984 78.5 0.1330508 | 10 950 320 251.2 -0.2279 -0.015 50.24 0.07036 | 25 610 700 549.5 1.42048 0.18916 109.9 0.14537 | 0 1290 30 23.55 -1.48155 4.71 0.0057 | 0 1205 75 58.875 0.13083 -0.785 -0.2303 11.775 0.01337 | 0 1175 170 133.45 0.23305 26.69 0.02824 | 10 1070 200 157 0.05962 0.13724 31.4 0.03066 | 20 1155 190 149.15 -0.02855 0.09119 29.83 0.02765 |

| CALCAMITE TANKS: AREA: DATE DAYS CUMULAT. DAYS | 1.2m DIAM 1.130976 | 05/12/93 0 0 | 08/12/93 92 92 | 11/30/93 109 201 | 02/25/94 71 272 | 06/15/94 110 382 | 08/05/94 51 433 | 12/14/94 131 564 | 02/14/95 62 626 | 04/07/95 52 678 | 06/06/95 60 738 | 10/03/95 119 857 ' |
|---|-----------------------|--------------------------|---|---|---|---|--|--|--|--|--|---|
| 1738 NO. OF USERS | | ADULT 5 | CHILDRE 1 | N | AREA: | 1.13 | | | | | | |
| SCUM FLUID SLUDGE SLUDGE VOL. (LT/P) ST-RATE LT-RATE XLT-RATE | | 0 0 0 0 | 0 670 215 40.49167 0.440127 | 0 855 300 56.5 0.1468654 0.2810945 | 0 840 300 56.5 0 | 1 800 265 49.908333 -0.0599242 -0.036418 | 0 530 190 35.783333 -0.2769608 | | | 5 800 130 24.483333 -0.1448718 -0.0247807 | 5 720 200 37.666667 0.2197222 0.0595307 | 25 220 30 5.65 -0.2690476 -0.1052142 |
| 1739 NO. OF USERS | | ADULT 4 | CHILDRE 1 | N | AREA: | 1.13 | | | | | | |
| SCUM FLUID SLUDGE SLUDGE VOL. (LT/P) ST-RATE LT-RATE XLT-RATE | | 0 885 225 50.85 | 0 770 300 67.8 0.184239 | 0 830 300 67.8 0 0.0843284 | 0 190 320 72.32 0.063662 0.0789338 | 0 535 340 76.84 0.0410909 0.0499448 | 0 395 180 40.68 -0.7090196 | 5 570 350 79.1 0.2932824 0.0124176 0.0232192 | 5 860 210 47.46 -0.5103226 | 10 250 50 11.3 -0.6953846 -0.5947368 | | 5 190 30 6.78 -0.1614286 -0.0252514 |

| CALCAMITE TANKS: AREA: | 1.2m DIAM 1.130976 | | | | | | | | | | | |
|---|-----------------------|--------------------------|--------------------------------------|---|---|---|---|---|---------------------------------------|--|--|---|
| DATE DAYS CUMULAT. DAYS | 05/ | /12/93 0 0 | 08/12/93 92 92 | 11/30/93 109 201 | 02/25/94 71 272 | 06/15/94 110 382 | 08/05/94 51 433 | 12/14/94 131 564 | 02/14/95 62 626 | 04/07/95 52 678 | 06/06/95 60 738 | 10/03/95 119 857 |
| 1740 NO. OF USERS | AD | OULT 2 | CHILDRE 1 | N | AREA: | 1.13 | | | | | | |
| SCUM FLUID SLUDGE SLUDGE VOL. (LT/P) ST-RATE LT-RATE XLT-RATE | | 0 830 195 73.45 | 0 760 180 67.8 -0.06141 | 0 805 140 52.733333 -0.1382263 -0.103068 | 0 810 200 75.333333 0.3183099 0.006924 | 0 905 160 60.266667 -0.1369697 0.0416206 | 0 530 190 71.566667 0.2215686 | 0 650 220 82.866667 0.0862595 0.1241758 0.0257991 | 0 700 255 96.05 0.2126344 | 0 245 60 22.6 -1.4125 -0.528655 | 0 715 90 33.9 0.1883333 -0.2814176 | 0 30 0 0 -0.2848739 -0.126257 |
| 1741 NO. OF USERS | AD | OULT 2 | CHILDRE 0 | N | AREA: | 1.13 | | | | | | |
| SCUM FLUID SLUDGE SLUDGE VOL. (LT/P) ST-RATE LT-RATE XLT-RATE | | 0 950 90 50.85 | 0 480 85 48.025 -0.03071 | 0 740 240 135.6 0.8034404 0.4216418 | 0 800 180 101.7 -0.4774648 0.1869485 | 0 400 140 79.1 -0.2054545 -0.3121547 | 0 110 65 36.725 -0.8308824 | 20 320 80 45.2 0.0646947 -0.1862637 -0.1934932 | | 10 80 25 14.125 -0.4889423 -0.2725877 | 10 235 65 36.725 0.3766667 -0.0487069 | 10 100 30 16.95 -0.1661765 0.0157821 |

| CALCAMITE TANKS: AREA: DATE DAYS CUMULAT. DAYS | 1.2m DIAM 1.130976 05/12/93 | | 11/30/93 109 201 | 02/25/94 71 272 | 06/15/94 110 382 | 08/05/94 51 433 | 12/14/94 131 564 | 02/14/95 62 626 | 04/07/95 52 678 | 06/06/95 60 738 | 10/03/95 119 857 |
|---|-----------------------------------|---------------------------------|---|--|--|--|------------------------|-----------------------|-----------------------|--|--|
| 1373 NO. OF USERS | ADULT | CHILDRE | N | AREA: | 1.13 | | | | | | |
| SCUM FLUID SLUDGE SLUDGE VOL. (LT/P) ST-RATE LT-RATE XLT-RATE | 693 363 137.483 | 760 260 97.93333 | 0 875 255 96.05 -0.0172783 -0.206136 | 0 895 230 86.633333 -0.1326291 -0.1869485 | 0 880 240 90.4 0.0342424 -0.0312155 | 0 830 290 109.23333 0.369281 | 1110 25 | - 0 | | 0 1020 150 56.5 0.6591667 0.2705939 | 5 125 0 0 -0.4747899 -0.0946927 |
| 1374 NO. OF USERS | ADULT | CHILDRE 0 | N | AREA: | 1.13 | | | | | | |
| SCUM FLUID SLUDGE SLUDGE VOL. (LT/P) ST-RATE LT-RATE XLT-RATE | 800 275 62.15 | 800 185 41.81 -0.22109 | 0 870 200 45.2 0.0311009 -0.0843284 | 0 875 250 56.5 0.1591549 -0.0207721 | 0 850 270 61.02 0.0410909 0.0874033 | 0 870 240 54.24 -0.1329412 | | 0 | | 0 500 100 22.6 0.1695 | 5 100 30 6.78 -0.1329412 -0.0315642 |

| | | | | * | | | | | | | | |
|---------------------------|-----------------------|----------|----------|------------|------------|-----------|------------|------------|------------|------------|------------|------------|
| CALCAMITE TANKS: AREA: | 1.2m DIAM 1.130976 | | | | | | | | | | | |
| DATE | | 05/12/93 | 08/12/93 | 11/30/93 | 02/25/94 | 06/15/94 | 08/05/94 | 12/14/94 | 02/14/95 | 04/07/95 | 06/06/95 | 10/03/95 |
| DAYS | | 0 | 92 | 109 | 71 | 110 | 51 | 131 | 62 | 52 | 60 | 119 |
| CUMULAT. DAYS | | 0 | 92 | 201 | 272 | 382 | 433 | 564 | 626 | 678 | 738 | 857 |
| 1372 | | ADULT | CHILDRE | EN | AREA: | 1.13 | | | | | | |
| NO. OF USERS | | 2 | 1 | | | | | | | | | |
| SCUM | | 0 | 0 | 0 | 0 | 0 | 0 | 10 | emptied | 10 | 5 | 0 |
| FLUID | | 0 | | 830 | 765 | 740 | 720 | 900 | | 300 | 800 | 145 |
| SLUDGE | | 0 | | 180 | 215 | 260 | 270 | 124 | | 45 | 60 | _ |
| SLUDGE VOL. (LT/P) | | 0 | | 67.8 | 80.983333 | 97.933333 | 101.7 | | 0 | | 22.6 | |
| ST-RATE | | | 0.61413 | 0.1036697 | 0.1856808 | 0.1540909 | 0.0738562 | | -0.7533333 | | 0.0941667 | -0.189916 |
| LT-RATE | | | | 0.3373134 | 0.00773.00 | 0.1664825 | | -0.2814652 | | -0.2610234 | 0.1205441 | -0.0946927 |
| XLT-RATE | | | | | 0.2977328 | | | -0.1173858 | | | -0.1385441 | |
| 1371 | | ADULT | CHILDRE | EN | AREA: | 1.13 | | | | | | |
| NO. OF USERS | | 6 | | | | | | | | | | |
| SCUM | | 0 | 0 | 0 | 0 | 10 | 20 | 10 | emptied | 50 | 5 | 10 |
| FLUID | | 440 | 570 | 645 | 575 | 390 | -(mixed) | 835 | - | 475 | 830 | 110 |
| SLUDGE | | 570 | 350 | 320 | 360 | 470 | - | 130 | - | 145 | 120 | 30 |
| SLUDGE VOL. (LT/P) | | 107.35 | 65.91667 | 60.266667 | 67.8 | 88.516667 | 0 | 24.483333 | 0 | 27.308333 | 22.6 | 5.65 |
| ST-RATE | | | | -0.0518349 | 0.1061033 | | -1.7356209 | | -0.3948925 | | -0.0784722 | -0.142437 |
| LT-RATE | | | | -0.2342454 | | 0.1560773 | | -0.3518315 | | 0.0247807 | | -0.1209963 |
| XLT-RATE | | | | | -0.1454044 | | | -0.1483447 | | | -0.0108238 | |
| | | | | | | | | | | | | |

| CALCAMITE TANKS: AREA: | 1.2m DIAM 1.130976 | | | | | | | | | | |
|---------------------------|-----------------------|------------|-----------|------------|-----------|-----------|------------|------------|-----------|-----------|------------|
| DATE | 05/12/9 | 3 08/12/93 | 11/30/93 | 02/25/94 | 06/15/94 | 08/05/94 | 12/14/94 | 02/14/95 | 04/07/95 | 06/06/95 | 10/03/95 |
| DAYS | | 0 92 | 109 | 71 | 110 | 51 | 131 | 62 | 52 | 60 | 119 |
| CUMULAT. DAYS | | 0 92 | 201 | 272 | 382 | 433 | 564 | 626 | 678 | 738 | 857 |
| 1368 NO. OF USERS | ADUL | CHILDRE | EN | AREA: | 1.13 | | | | | | |
| SCUM | | 0 0 | 0 | 0 | 0 | 0 | 0 | emptied | 10 | 0 | 10 |
| FLUID | 99 | 5 540 | 940 | 900 | 875 | 775 | 55 | - | 220 | 425 | 50 |
| SLUDGE | 10 | 5 140 | 210 | 100 | 240 | 130 | 35 | - | 45 | 80 | 20 |
| SLUDGE VOL. (LT/P) | 37.2 | 9 31.64 | 47.46 | 22.6 | 54.24 | 29.38 | 7.91 | 0 | 10.17 | 18.08 | 4.52 |
| ST-RATE | | -0.06141 | 0.1451376 | -0.3501408 | 0.2876364 | -0.487451 | -0.1638931 | -0.1275806 | 0.1955769 | 0.1318333 | -0.1139496 |
| LT-RATE | | | 0.050597 | | 0.0374586 | | -0.2545604 | | 0.0198246 | | -0.0315642 |
| XLT-RATE | | | | -0.0540074 | | | -0.077931 | | | 0.0584483 | |

MONITORING VIP LATRINES AT SOSHANGUVE

| Pit size: AREA: | 1m auger 0.785 | | | | | | | | | | | | | | |
|--|-------------------|------------------|---|-----------------------|---|---------|--|---------------------------|---------------------------------------|-----------------------------|--|-----------------------------|--------------------------------------|------------------------------|---|
| DATE DAYS CUMULAT. DAYS | 0 | | 09/21/93 42 95 | 11/25/93 65 160 | 02/11/94 78 238 | | 06/15/94 63 362 | 08/04/94 50 412 | 11/16/94 103 515 | 12/15/94 29 544 | 02/10/95 · 57 601 | 04/06/95 55 656 | 06/05/95 60 716 | 08/04/95 60 776 | 10/10/95 66 842 |
| 1277FF NO. USERS | ADULT 2 | CHILDRI 4 | | | | | | | | | | | | | |
| DEPTH ST-RATE LT-RATE | 1415 | 1400 0.037028 | | 1410 -0.02013 | 1380 0.050321 0.018298 | | 1300 0.072685 0.084409 | 1335 -0.09158 | 1275 0.07621 0.02138 | 1200 0.338362 | 1215 -0.03443 0.09128 | 1175 0.095152 | 1050 0.27257 0.18772 | 1020 0.065417 | 1000 0.0396465 0.051918 |
| DELTA SLUDGE | | 1.9635 | | 0.6545 | | 10.472 | 15.0535 | 10.472 | | 28.1435 | | 31.416 | 47.7785 | 51.7055 | 54.3235 |
| 1278FF NO. USERS | ADULT 2 | CHILDRE 3 | | no change | ; | | | | | | | | | | |
| DEPTH ST-RATE LT-RATE DELTA SLUDGE | 1495 | 0.266604 | 1315 0.336429 0.297474 28.2744 | 1285 0.072462 | 1240 0.090577 0.082343 | 0.12869 | 1200 -0.02492 0.050645 | 1130 0.2198 57.3342 | 0.12827 | 1070 0.027069 66.759 | 1070 0 0.00913 66.759 | | 970 -0.02617 0.13652 82.467 | | 890 0.0237879 0.0996825 95.0334 |
| 1279FF | ADULT | CHILDRE | | 32.9000 | 40.0334 | 47.9094 | 15-06-94 | \$1.3342 | 03.9730 | 00.739 | 00.739 | 84.0378 | 82.407 | 93.4020 | 95.0334 |
| NO. USERS DEPTH ST-RATE LT-RATE DELTA SLUDGE | 2 1700 | 1615 0.314741 | 1575 0.186905 0.258224 24.54375 | | 1570 0.050321 0.006862 25.5255 | 0.04826 | 2 1660 -0.32708 -0.14244 7.854 | 1560 0.3925 27.489 | 1505 0.10479 0.19882 38.2883 | 1450 0.372198 49.0875 | 1490 -0.13772 0.03423 41.2335 | | 1460 0.09813 0.0512 47.124 | 1440 0.065417 51.051 | 1440 0 0.0311508 51.051 |
| 1280FF NO. USERS DEPTH ST-RATE LT-RATE DELTA SLUDGE | ADULT 2 1620 | 1500 0.888679 | 21-09-92 2 1315 1.728869 1.260132 119.7735 | | 0.411713 | | 1390 -0.03115 -0.7122 90.321 | | 1385 0.13337 0.01283 92.2845 | 1320 0.879741 117.81 | -0.06846 | 1360 0.285455 102.102 | 0.27304 | 1315 0.032708 119.7735 | 1310 0.0297348 0.0311508 121.737 |

MONITORING VIP LATRINES AT SOSHANGUVE

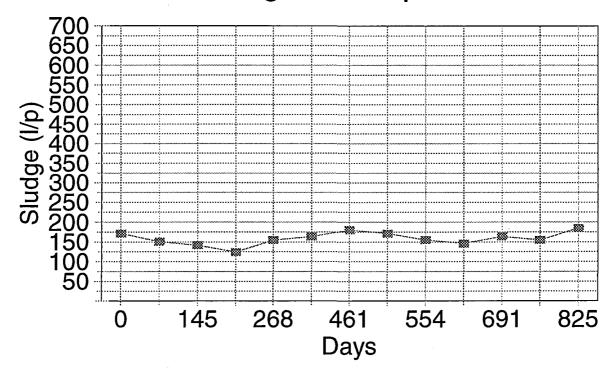
| Pit size: AREA: | 1m auger 0.785 | | | | | | | | | | | | | | |
|---|-------------------|------------------|--|---|--|-----------------------------|--|----------------------------|---------------------------------------|------------------------------|---------------------------------------|------------------------------|--|----------------------------|--|
| DATE DAYS CUMULAT. DAYS | 0 | | 09/21/93 42 95 | 11/25/93 65 160 | 02/11/94 78 238 | 04/13/94 61 299 | 06/15/94 63 362 | 08/04/94 50 412 | 11/16/94 103 515 | 12/15/94 29 544 | 02/10/95 57 601 | 04/06/95 55 656 | 06/05/95 60 716 | 08/04/95 60 776 | 10/10/95 66 842 |
| 1295FF NO. USERS | ADULT 4 | CHILDRE 3 | EN | | | | | | | | | | | | |
| DEPTH ST-RATE LT-RATE DELTA SLUDGE | 1820 | 1730 | 1735 -0.01335 0.100338 9.537 | 1745 -0.01725 8.415 | 1490 0.366621 0.192133 37.026 | 1665 -0.32172 17.391 | 1560 0.186905 -0.06331 29.172 | 1545 0.033643 30.855 | 1425 0.13065 0.09895 44.319 | 1460 -0.13534 40.392 | 1410 0.09837 0.01956 46.002 | 1350 0.122338 52.734 | 1200 0.28036 0.20478 69.564 | 1340 -0.26167 53.856 | 1100 0.4077922 0.0890023 80.784 |
| 1312FF NO. USERS | ADULT 2 | CHILDRE 2 | | no change | ; | | | | | | | | | | |
| DEPTH ST-RATE LT-RATE DELTA SLUDGE | 1645 | | 1525 0.046726 0.247895 23.562 | | 1190 0.679327 0.459747 89.33925 | | -0.85464 | | 0.03207 | 1740 -0.23685 -18.6533 | -0.06846 | 1700 0.124886 -10.7993 | 0.00853 | | 1700 -0.0892045 0.0467262 -10.79925 |
| 1313FF NO. USERS | ADULT 2 | CHILDRE 2 | | no change | | | | | | | | | | | |
| DEPTH ST-RATE LT-RATE DELTA SLUDGE | 2120 | 2020 0.370283 | 1985 0.163542 0.278882 26.50725 | 1800 0.558558 | 1545 | 2035 -1.57643 16.6898 | 2020 0.046726 -0.75176 19.635 | | 1905 0.08574 0.14751 42.2153 | 1880 0.169181 47.124 | 1835 0.15493 0.15974 55.9598 | 1800 0.124886 62.832 | 1900 -0.32708 -0.11092 43.197 | 1860 0.130833 51.051 | 1840 0.0594697 0.0934524 54.978 |
| 1314FF NO. USERS | | CHILDRE | | no oboneo | | | | | | | | | | | |
| DEPTH ST-RATE LT-RATE DELTA SLUDGE | 2 1475 | 1450 | 1400 0.311508 0.206579 | no change 1360 0.161026 30.107 | 1025 | 1340 -1.35123 35.343 | 1370 -0.1246 -0.72802 27.489 | 1400 -0.157 19.635 | 1355 0.11432 0.02565 31.416 | 1330 0.225575 37.961 | 1320 0.04591 0.10649 40.579 | 1170 0.713636 79.849 | 1200 -0.13083 0.27304 71.995 | 1200 0 71.995 | 1200 0 0 71.995 |

MONITORING VIP LATRINES AT SOSHANGUVE

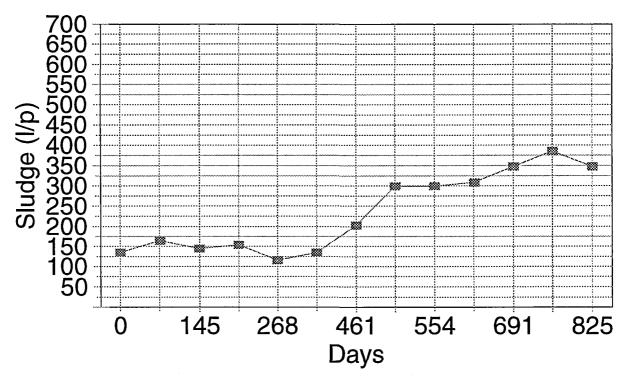
| Pit size: AREA: | 1m auger 0.785 | | | | | | | | | | | | | | |
|---------------------|-------------------|----------------|----------------|----------------|----------------|----------------|----------------|----------------|-----------------|----------------|----------------|----------------|----------------|----------------|----------------|
| DATE DAYS | 06/17/93 0 | 08/10/93 53 | 09/21/93 42 | 11/25/93 65 | 02/11/94 78 | 04/13/94 61 | 06/15/94 63 | 08/04/94 50 | 11/16/94 103 | 12/15/94 29 | 02/10/95 57 | 04/06/95 55 | 06/05/95 60 | 08/04/95 60 | 10/10/95 66 |
| CUMULAT. DAYS | 0 | 53 | 95 | 160 | 238 | 299 | 362 | 412 | 515 | 544 | 601 | 656 | 716 | 776 | 842 |
| 1315FF NO. USERS | 4 | CHILDRE 2 | 2 | 21-09-94 | | | | | | | | | | | |
| DEPTH | 1005 | 940 | 915 | 925 | 865 | 930 | | 880 | 865 | 860 | 840 | 840 | 840 | | replaced wi |
| ST-RATE | | 0.160456 | | -0.02013 | 0.100641 | -0.13941 | 0.041534 | 0.0785 | | 0.022557 | 0.04591 | 0 | 0 | -0.06542 | 1.7246212 |
| LT-RATE | | | 0.123947 | 16 700 | 0.045746 | 147060 | -0.04748 | 24 5 4275 | 0.03848 | 20 47075 | 0.03803 | 22 20775 | 0 | 26 50725 | 0.8722222 |
| DELTA SLUDGE | | 8.5085 | 17.6715 | 15.708 | 27.489 | 14.7263 | 18.05325 | 24.54375 | 27.489 | 28.47075 | 32.3978 | 32.39775 | 32.39/8 | 26.50725 | 197.33175 |
| 1316FF | ADULT | CHILDRE | EN | | | | | | | | | | | | |
| NO. USERS | 2 | | | no change | : | | | | | | | | | | |
| DEPTH | 1075 | | 1020 | 985 | 870 | 960 | 1090 | 1120 | 1155 | 1160 | 1050 | 945 | 1030 | 1080 | 945 |
| ST-RATE | | 0.22217 | -0.07476 | 0.084538 | 0.231474 | -0.23164 | -0.32397 | -0.0942 | -0.05335 | -0.02707 | 0.30298 | 0.299727 | -0.22242 | -0.13083 | 0.3211364 |
| LT-RATE | | | 0.090895 | | 0.164685 | | -0.27855 | | -0.0667 | | 0.19169 | | 0.0273 | | 0.1059127 |
| DELTA SLUDGE | | 11.781 | 8.6394 | 14.1372 | 32.2014 | 18.0642 | -2.3562 | -7.0686 | -12.5664 | -13.3518 | 3.927 | 20.4204 | 7.0686 | -0.7854 | 20.4204 |
| 292FF NO. USERS | ADULT | CHILDRE | EN | | | | | | | | | | | | |
| DEPTH | 2700 | 2570 | 2500 | 2100 | 1300 | 1480 | 1560 | 1730 | 1735 | 1180 | 1890 | 1560 | 1800 | 1950 | 1985 |
| ST-RATE | | 0.481368 | 0.327083 | 1.207692 | 2.012821 | -0.5791 | -0.24921 | -0.66725 | -0.00953 | 3.755819 | -2.44452 | 1.1775 | -0.785 | -0.49063 | -0.104072 |
| LT-RATE | | | 0.413158 | | 1.646853 | | -0.41149 | | -0.22447 | | -0.35371 | | 0.15359 | | -0.2881448 |
| DELTA SLUDGE | | 25.5255 | 39.27 | 117.81 | 274.89 | 239.547 | 223.839 | 190.4595 | 189.478 | 298.452 | 159.044 | 223.839 | 176.715 | 147.2625 | 140.39025 |

WARDEN: 7de Laan, no. 6

Sludge build up

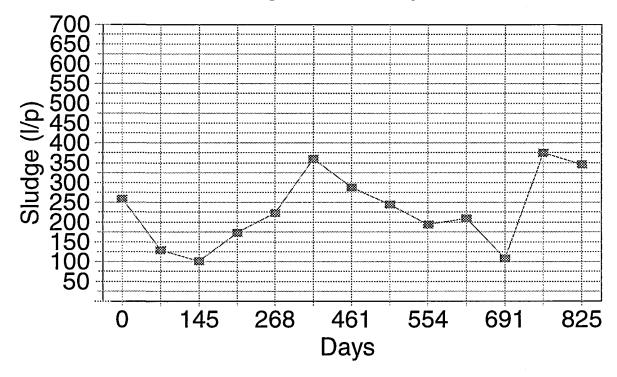


WARDEN: 7th Ave, no. 8

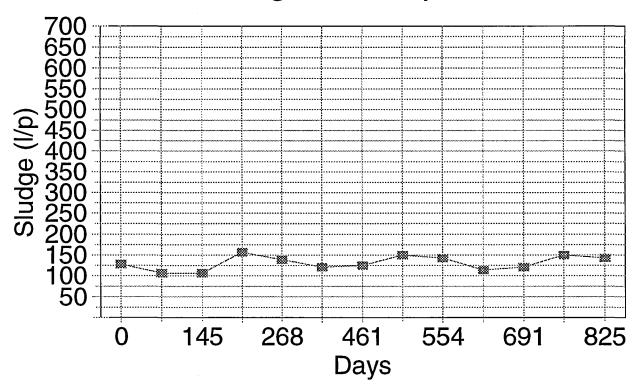


WARDEN: 7th Ave, no. 10

Sludge Build up

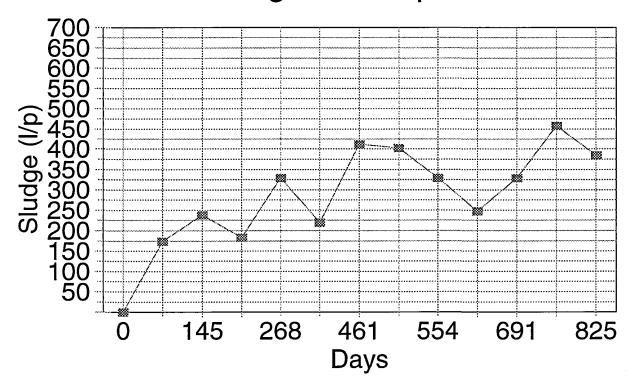


WARDEN: 7th Ave, no. 12

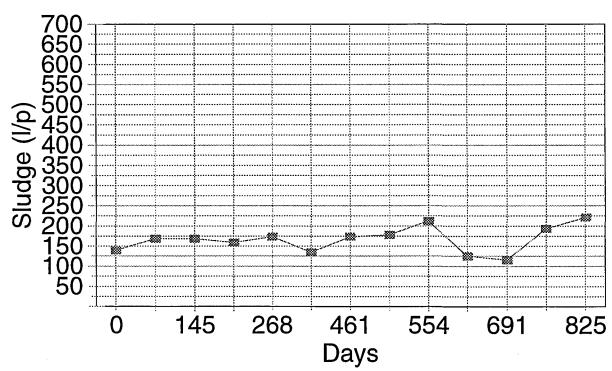


WARDEN: c/o 7th + Park

Sludge Build up

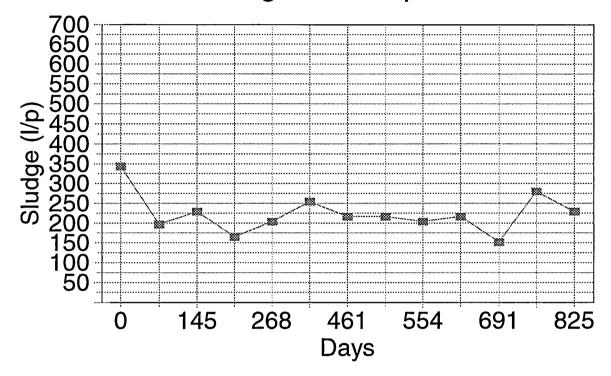


WARDEN: c/o 8th + Park

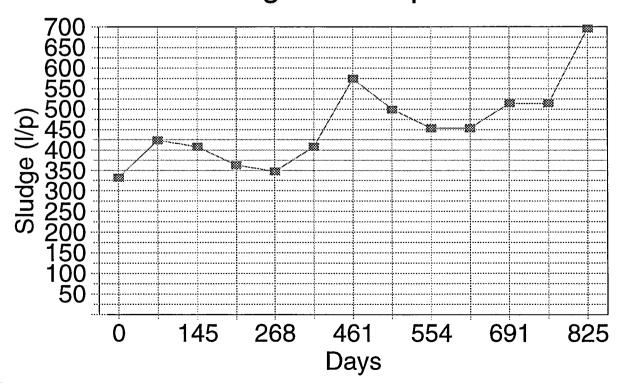


WARDEN: 8th Ave, no. 13

Sludge Build up

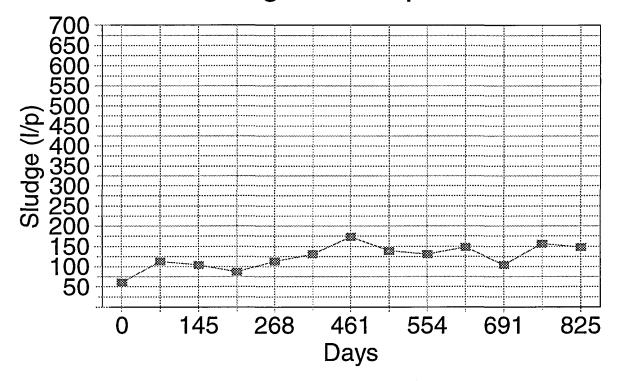


WARDEN: 8th Ave, no. 7

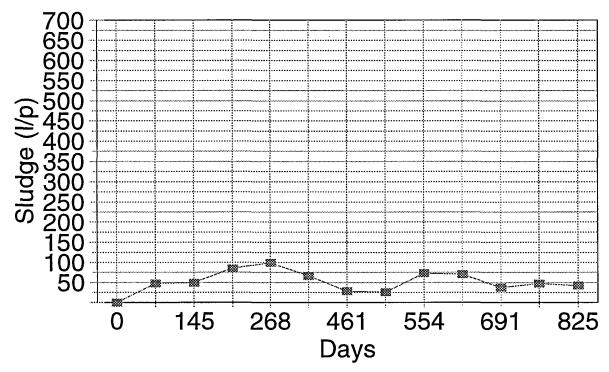


WARDEN: 8th Ave, no.3

Sludge Build up

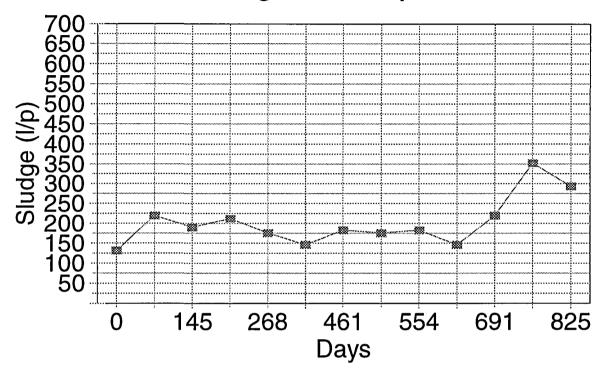


WARDEN: Boarding House

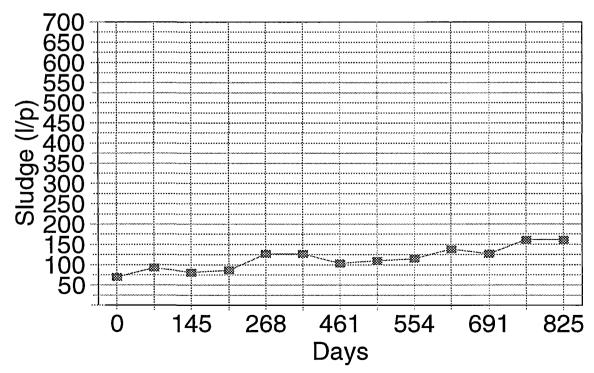


WARDEN: 7th Ave, no. 20

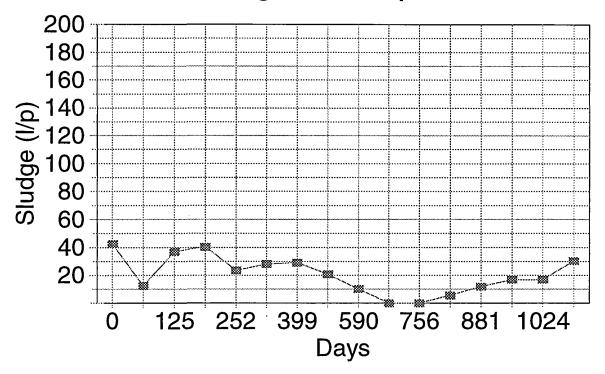
Sludge Build up



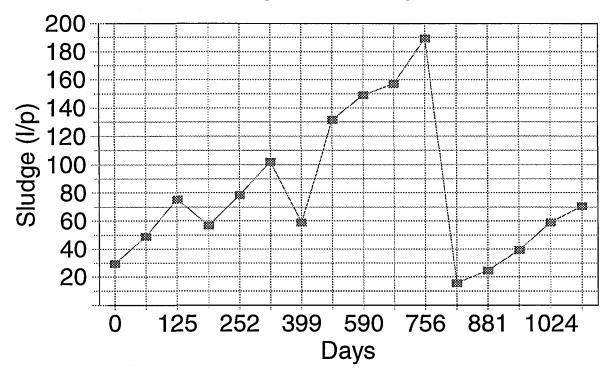
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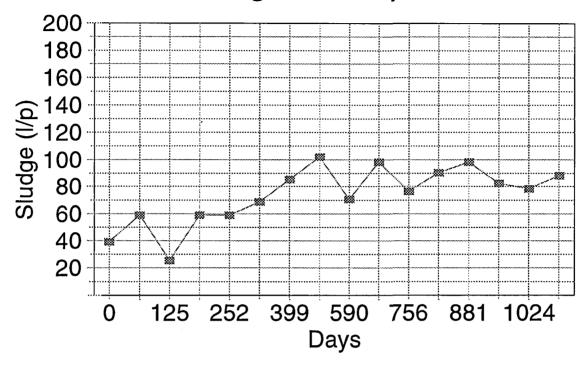
Sludge Build up



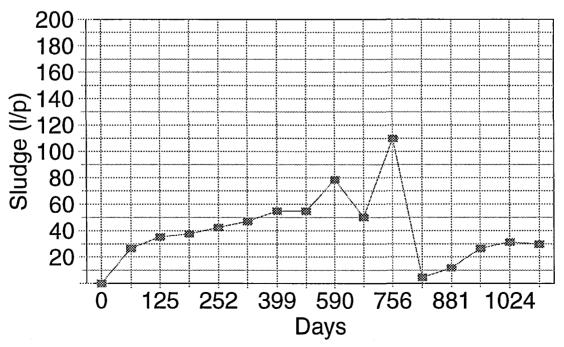
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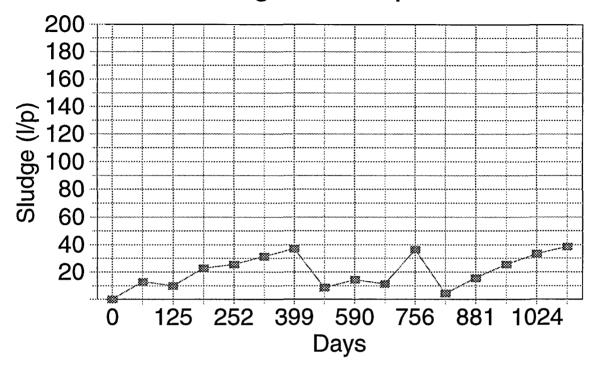
Sludge Build up



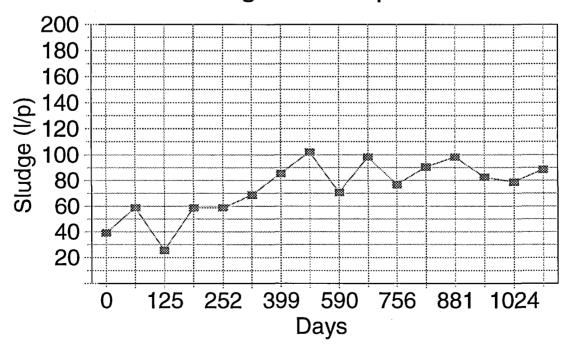
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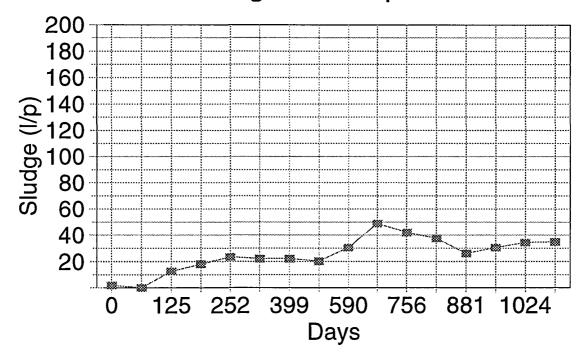
Sludge Build up



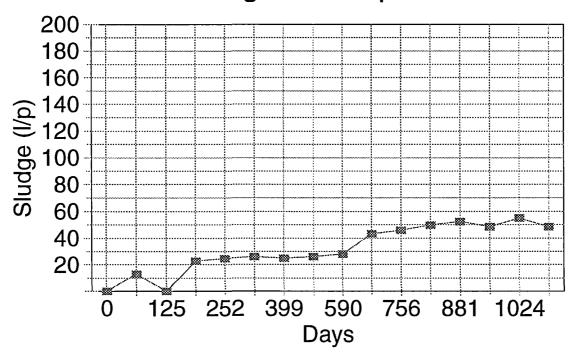
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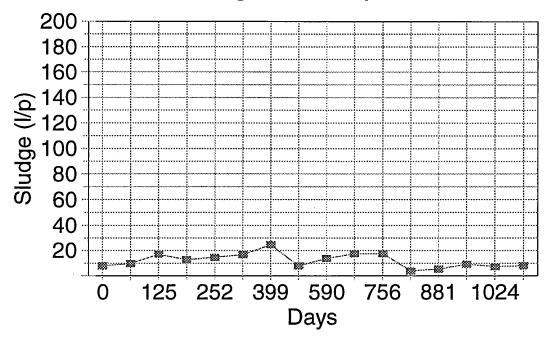
Sludge Build up



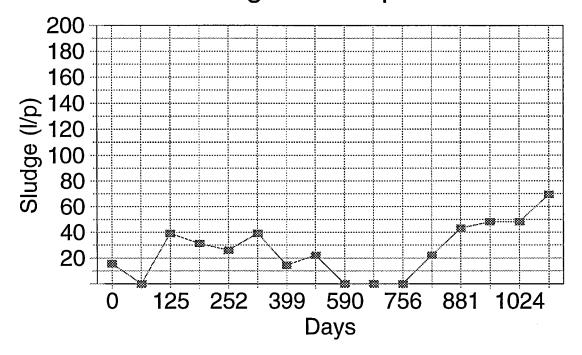
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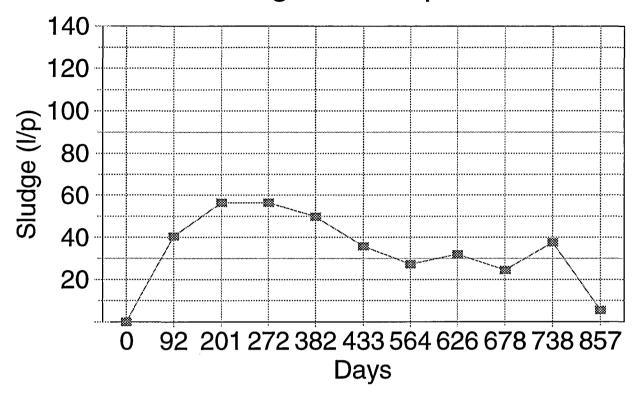
Sludge Build up



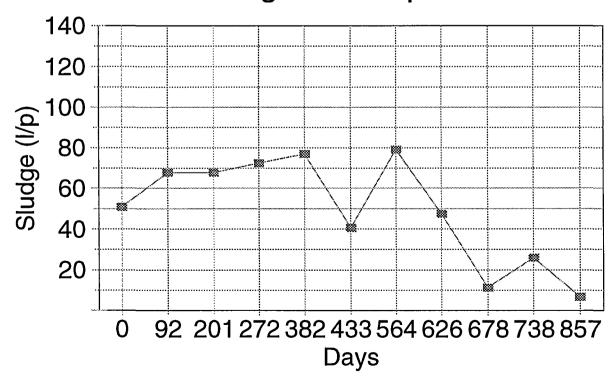
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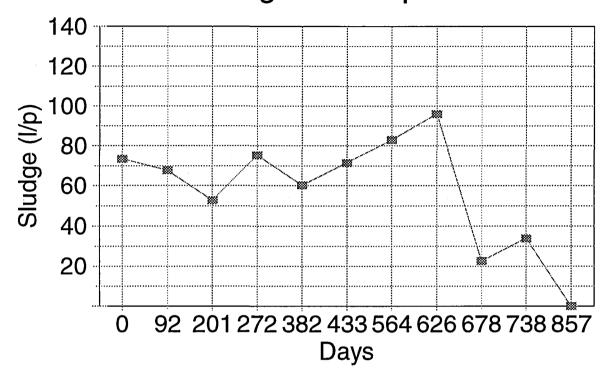
Sludge Build up



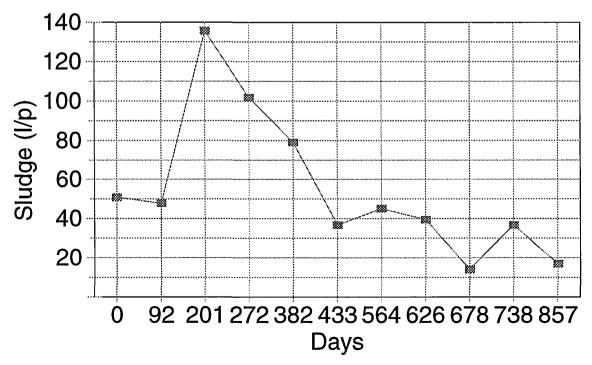
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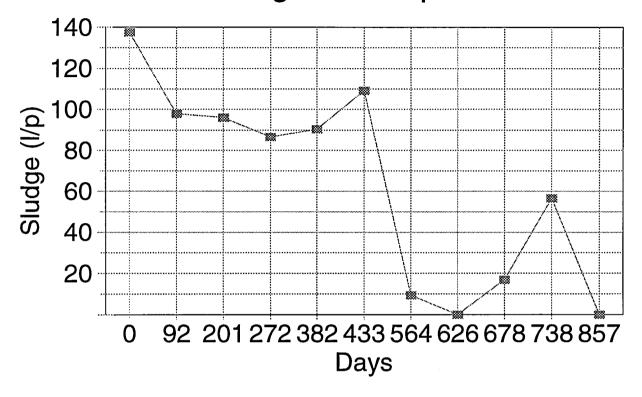
Sludge Build up



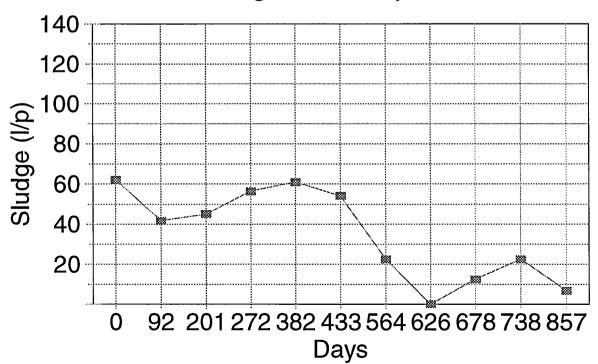
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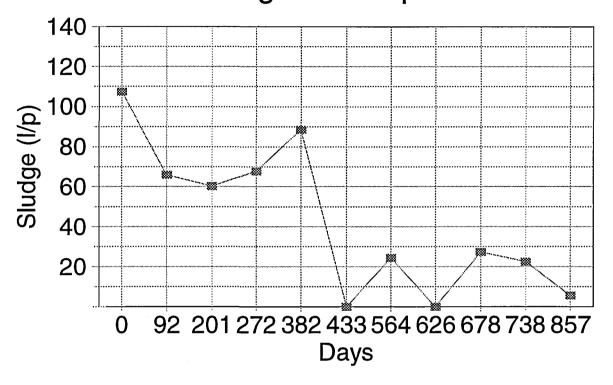
Sludge Build up



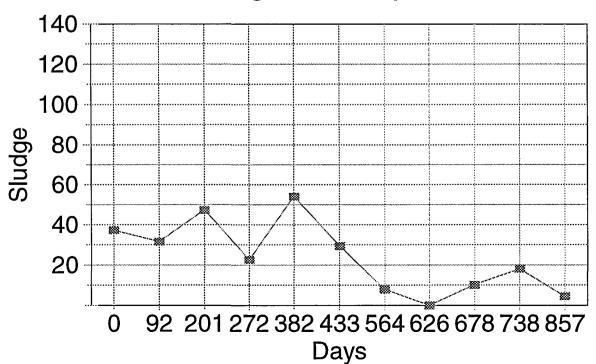
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Sludge Build up

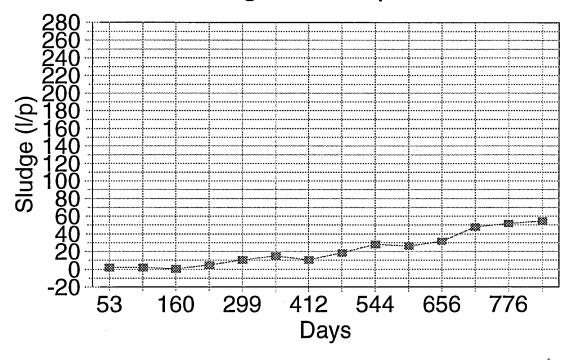


IVORY PARK: 1368

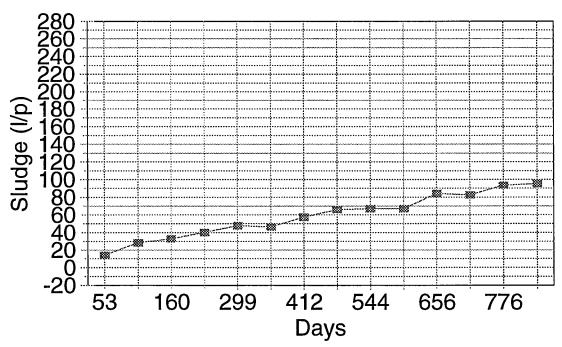


SOSHANGUVE: 1277FF

Sludge Build up

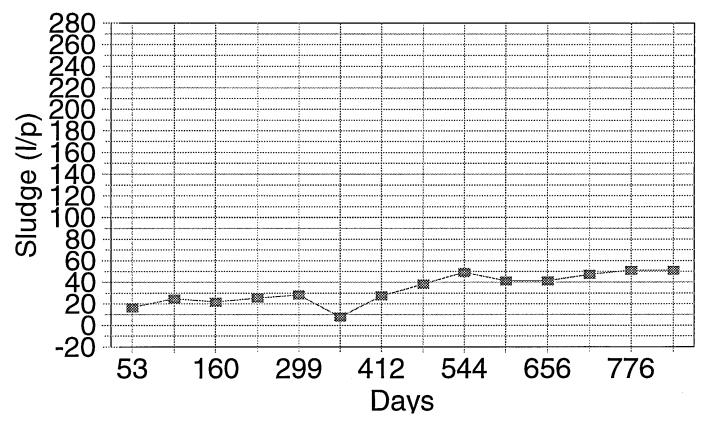


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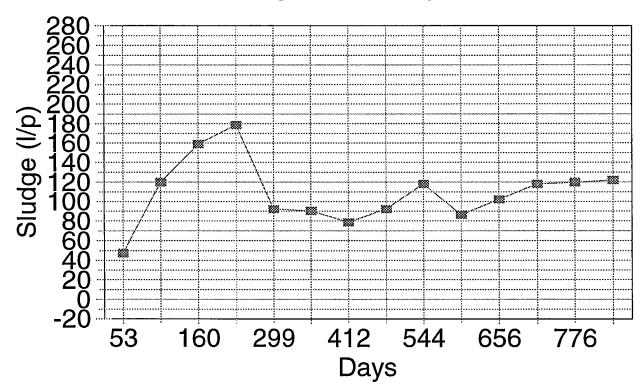


SOSHANGUVE: 1279FF

Sludge Build up

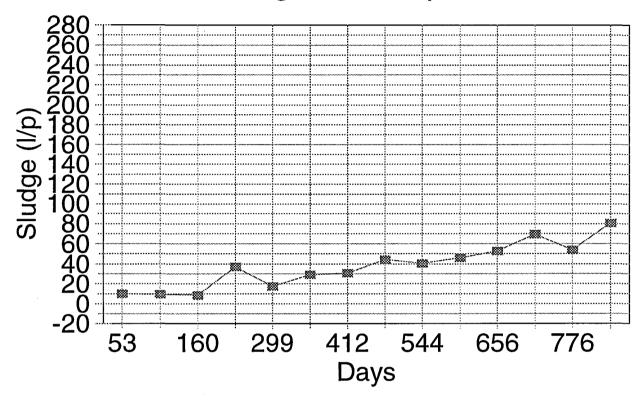


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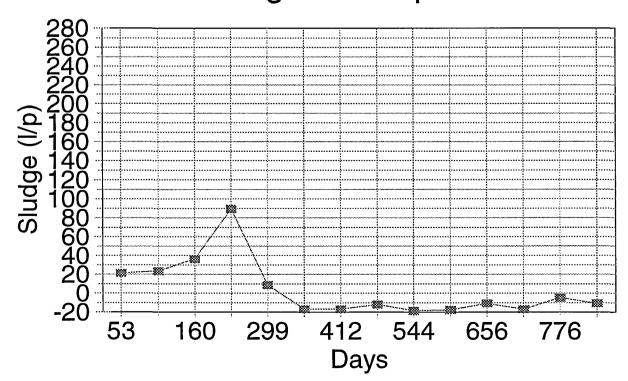


SOSHANGUVE: 1295FF

Sludge Build up

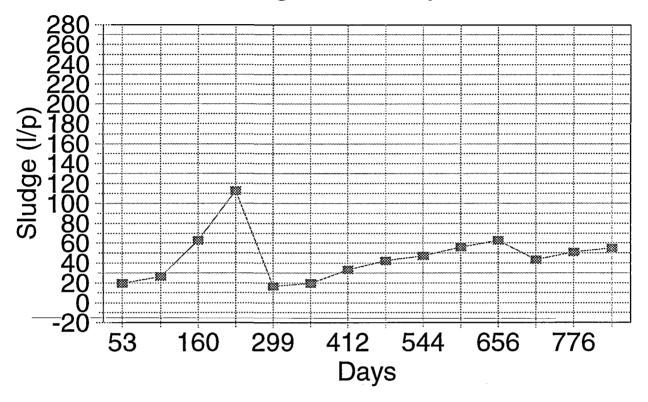


SOSHANGUVE: 1312FF

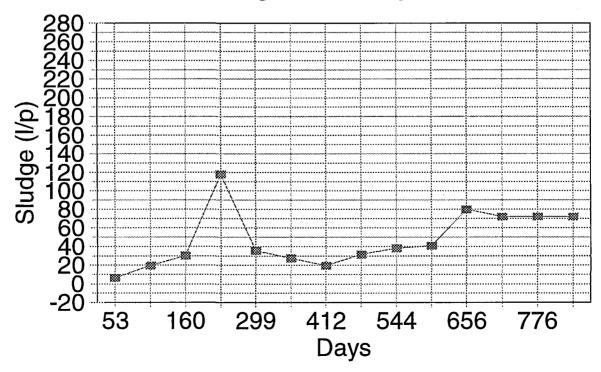


SOSHANGUVE: 1313FF

Sludge Build up

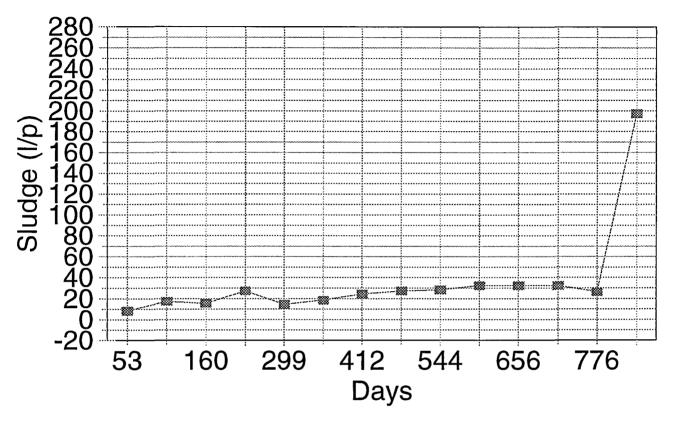


SOSHANGUVE: 1314FF

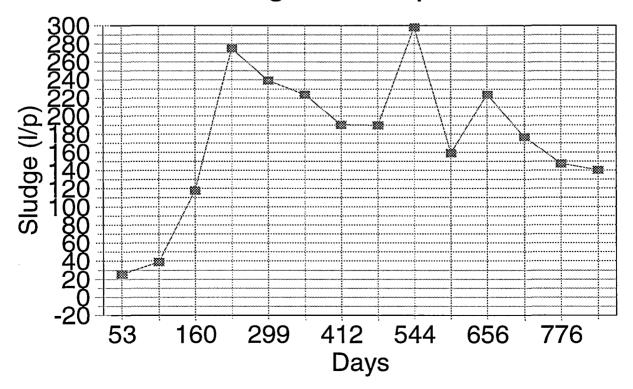


SOSHANGUVE: 1315FF

Sludge Build up



SOSHANGUVE: 292FF



APPENDIX III

Notes on some STED systems

Notes taken during discussion with Ronnie Crouse at the CPA offices in PE on 1994/04/03.

Marselle

- Ronnie Crouse direct telephone number; (041)390 2088
- Number of office at Marselle; (0464)81243
- Most of the Municipalities that the CPA deals with have insufficient funds for maintenance of the services infrastructure. Result is that no maintenance is done in these areas.
- In Marselle only one type of tank was installed. Most of the systems that we are monitoring are the so called dry systems. The Pan is a ceramic pan manufactured by Vaal potteries for the system supplier. The pan has no trap and discharges vertically into a curved pipe which enters the tank below the water level. A wash trough was installed on the outside of the toilet building which drained into the tank via the toilet pan. The CPA has found that these systems did not perform satisfactorily at Marselle. There was no problem with the system itself but it seemed as if there was insufficient water for proper operation. The tanks became like Pit latrines with a very thick sludge. In Marselle the people had to fetch water from standpipes some distance away. It is unlikely that people used the wash trough to dispose of water. The result was that only faeces and urine were deposited in the tank. To date 220 sites have been converted from dry to wet systems and all are now working well.
- Before the systems were converted average water consumption in Marselle was only about 10litres per capita per day.
- There were many blockages on the bend into the tank. The dry system is supplied with a plunger rod to assist with getting the solid waste into the tank. They normally recommend that the system is rodded at least once per day. It appears as if even with this rodding the dry systems at Marselle were blocking.
- The residents do not have sufficient money to pay for the emptying of the tank by vacuum tanker so they generally remove the T piece and then empty the tank manually. They then omit to replace the T piece resulting in the scum and floating solids draining into the solids free sewer.
- In Marselle water pumps were installed in the pumpstation. There were a number of problems with these blocking. CPA have now replaced these with sewage pumps and they are now running smoothly. These problems were mainly associated with solids entering the system as a result of the failed dry systems. Ronnie said that the water pumps might have worked if the dry systems had not failed but he would still recommend that sewage pumps are installed in future schemes. He says that you do get some sludge collecting in the sump even now with the dry systems mostly converted to wet systems. This might be suspended solids dropping out in the sump but it could also be slime that might build up in the sewers and then sloughing off the pipes.

- CPA have now bought a high pressure pump to use when cleaning out the tanks. (Kranzle profi-jet) This pump uses a venturi to suck the contents out of the tank. They will also use this to clean the sewer pipes if necessary.
- CPA persons on site: Leon Oosthuizen who runs the office and Dennis Botha who made the changes to convert the systems from dry to wet.
- They are now extending Marselle and installing another 120 new wet systems.
- CPA are now getting applications for developments where applicants would like to apply for housing subsidies. Ronnie is looking for ways to promote STED sanitation with the consulting engineers.
- The town of Hermanus was also on conservancy tanks which will now be converted to STED similar to Warden.
- Aberdeen will also be installing STED sanitation. The tender designs are now being prepared.

Cathcart

- CPA is presently installing a STED system in Cathcart.
- Consultants were briefed to prepare two separate designs. One conventional
 waterborne and the other STED. Steve Landoldt of Cahi de Vries in Bisho did
 the design. Both schemes went to tender but the STED system was cheaper
 probably because site is very rocky
- Tender prices as follows; Single toilet block R480+VAT. Septic tank R1203+VAT +toilet pan & washtrough.

General notes relating to the site visit at Marselle

- Some of the systems were originally dry systems but the CPA is now replacing them with a plastic toilet pan with a flush of about 3-4 litres. Note that the original tank is left and only the pan and connecting pipework is altered. The original installation was with a ceramic pan.
- The residents say that the tank was emptied when the new pans were installed but in discussion with the CPA labour it seems as if the liquid layer in the tank was pumped to below the level of the outlet T piece so that they could work on the tank pipework. It seems as if the sludge layer was in most cases left undisturbed.
- The reason given for the replacement of the old dry pans was that all the problems with the sewer network were associated with the dry systems. The CPA says that in their opinion based on their experience at Marselle there should be some addition of water to these systems.

GAVIN NORRIS

APPENDIX IV

NOTES ON SANITATION SYSTEMS AT UMBUMBULU

REPORT ON VISIT TO UMBUMBULU IN FEBRUARY 1995

Background

On the 16 & 17 February 1995 a team from CSIR consisting of Gavin Norris and Andy Murdoch visited several houses at Umbumbulu that have Biotag sanitation systems. On the 17th they were joined by Gordon Upton of Shayamanzi, Maurice Curtis of Fibreform and Chris Morris of CSIR. The primary purpose of the visit was to measure the sludge accumulation in 10 of the Biotag tanks in section C Folweni as part of the ongoing monitoring programme for a Water Research Commission project. A secondary purpose was to examine the Biotag systems to see how well they had stood up to several years of use by typical families in Umbumbulu.

Findings

Some of the tanks had been pumped out since our last visit which was on the 8th of December 1994. When asked, the residents said that this was done just before Christmas and that the pumping was done by Kwazulu Finance Corporation. This is a normal operational requirement for on-site sanitation systems. It can be expected that a system such as the Biotag with a 1 000 litre tank would require emptying at least once every five years.

Samples of the tanks' contents were drawn using a transparent tube developed by the CSIR. All of the tanks appeared to be operating very well with a clear separation between the sludge layer at the bottom of the tank and a relatively clear layer of liquid above this sludge layer. Some of the tanks had a floating scum layer forming on the surface of the liquid.

At three of the houses it was noticed that the gulleys were overflowing. Note that this does not indicate any problem with the sanitation system itself because at Umbumbulu only the toilet wastes are drained into the Biotag tanks. Kitchen and bathroom wastes bypass the tanks and drain directly into the soakaways. It would appear as if the fatty wastes, particularly from the kitchens, have caused the soakaways to become blocked. This viewpoint is supported by the fact that one of the residents whose soakaway had been excavated told us that it was filled by a substance that resembled candle wax. The blockage of these soakaways is a cause for concern because the grey water from the kitchens and bathrooms is overflowing from the gulleys and forming puddles on the ground. Since the partially treated effluent from the tanks is also disposed of in the soakaways, this effluent could rise to the ground surface. However, without a more detailed investigation which would include excavation of several blocked soakaways, it is impossible to determine the exact cause for the failure of the soakaways. It would appear at this stage that there are three possibilities for preventing this problem from

occurring in the future. The first would be to construct larger soakaways. The second is to install a grease trap between the gulley and the soakaway. This would result in the trap collecting the grease, and if this becomes blocked then it is easily cleaned. Note that if the problem of blocked gullies is more widespread, then this might be a way of rectifying the problem with limited expenditure. The third option would be to put all the wastes through the Biotag tank, which would capture all the greases into a floating scum layer. The writer does not believe that this would have any serious effects on the operation of the tanks but has not yet had the opportunity to test this opinion with a microbiologist. Before this option is tried in practice it needs to be thoroughly discussed.

Most of the pedestals inspected were in good condition. There were no smells coming from any of the toilets. The flap of one of the units had broken. The woman of the house said that she was cleaning the toilet and it just broke. What was noticeable was the fact that even though there was no flap and therefore no water seal, there were still no smells in the bathroom, even though this was a "through the wall" unit.

The washers in some of the cisterns have failed. This means that when the residents fill the cistern, all the water immediately drains through the toilet into the tank. The people are all flushing the toilets manually with small water containers. Replacing these washers is a simple task which should be a normal maintenance operation on standard toilet cisterns.

Residents were unsure of where they could go to obtain advice and assistance when there were problems with the sanitation systems. It seemed as if there was not any functioning local authority responsible for the operation and maintenance of the services in Umbumbulu. For the proper functioning of any sanitation system this is essential. If Umbumbulu were served with waterborne sanitation, there would be a disastrous situation with raw sewage running down the streets.

One of the causes for concern was the apparent lack of user understanding of the operation of the toilet system. Some of the residents were adding chemicals to the unit because they were not aware that with these types of system it was better not to add anything. It is recommended that whatever type of sanitation system is installed, proper user education is carried out and that one of the local residents or the local authority in each area be trained on the systems so that they can answer any queries.

Conclusions

- 1. On the whole, the Biotag units at Umbumbulu are operating satisfactorily.
- 2. More user education is required when installing any sanitation system.
- 3. It is essential that there is a competent local authority to maintain any sanitation system.
- 4. Fats and greases from the kitchen are causing the soakaways to fail. This can most easily be rectified by installing grease traps.

GAVIN NORRIS

APPENDIX V

Comments received from Allan Batchelor, Environmentek

The observations that you have documented re an inverse correlation between sludge depth and number of users correlates with observations I made in two independent studies, one funded by Calcamite and restricted to Calcamite tanks, and the other funded by TPA through Laubscher, Human & Lombard.

The precise reasons for this apparent anomaly has to my knowledge never been critically examined and as such one can only speculate as to the reason. My own feelings are that:

- The flush volume is too low given the high organic and ammonia load on systems serving more than three people, and this could effect the biophysical processes including separation of the solid/liquid fraction. Most aquaprivies are fed with both flush water and additional water from washing facilities. I personally feel that the volume of water needed to ensure dilution and methanogenesis has not been evaluated properly, with the focus on our local systems being water conservation rather than a balance between flush volume and process requirements.
- 1.1 The reasons that I feel this, are anecdotal. As early as 1914 it was found that when buckets containing sewage were introduced into the sewage treatment system at Daspoort, the biological processes were adversely affected unless the bucket emptying was followed by copious washing of the buckets to in effect dilute the effluent.
- 1.2 The information that I copied to you re piggeries effluent, that solids separation in pig waste failed unless the quantity of water added was "sufficient". (Ref. Separation of Solid and Liquid Parts of Pig Slurry. J C Glerum, G Klomp and H R Poelma. Livestock Waste Management).
- 2. The tank size is too small for greater than 3-4 users resulting in insufficient residence time for anaerobiasis to develop. My feeling is that all the systems exist in a state of acid fermentation, giving rise to odours.
- 2.1 The contents of all low-volume flush toilets sampled by ourselves during the surveys and three samples brought to me yesterday, showed o signs of typical anaerobiasis, i.e. there was not the slightest smell of methane or hydrogen sulphide. The samples all smelt of fresh faeces, which to me indicates that the residence time necessary for some form of digestion is simply not being met, although the possibility exists that the digestion process is being inhibited by something (possibly ammonia). This may also influence the settling characteristics of the contents.

Note: This could also be aggravated by the fact that the tanks are emptied fairly often but are never refilled with water afterwards. The only liquid that enters the tanks is flushing/washing water or urine.